AISI 1090M
Accelerated Stab Bar Steel
Iteration #9

Fatigue Behavior, Monotonic Properties
and
Microstructural Data

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SUMMARY

The required chemical analysis, microstructural data, mechanical properties, cyclic stress-strain data and strain-controlled fatigue data for AISI 1090M (GM) Hot Form-Accelerated Cooled steel (Iteration # 9) have been obtained. The material was provided by the American Iron and Steel Institute (AISI) in the form of metal bars. These bars were machined into smooth axial fatigue specimens. A monotonic tensile test was performed to measure yield strength, tensile strength and reduction of area. Nineteen specimens were fatigue tested in laboratory air at room temperature to establish a strain-life curve.

INTRODUCTION

This report presents the results of tensile and fatigue tests performed on a group of 20 1090M (GM) Hot Form-Accelerated Cooled steel samples. The material was provided by the American Iron and Steel Institute.

The objectives of this investigation were to obtain a chemical analysis, and the microstructural data, mechanical properties, cyclic stress-strain data and strain-life tests requested by the AISI bar group.

EXPERIMENTAL PROCEDURE

Specimen Preparation

The material for the study was received in the form of bars. Smooth cylindrical fatigue specimens, shown in Figure 1, were machined from the metal bars. The gauge sections of the fatigue specimens were mechanically polished in the loading direction using 240, 400, 500, and 600 emery paper. After polishing, a thin band of M-coat D acrylic coating was applied along the central gauge section. The purpose of the M-coat D application was to prevent scratching of the smooth surface by the knife edges of the strain extensometer, thus reducing the incidence of knife-edge failures. In total, 19 fatigue data points were generated.

Test Equipment and Procedure

A monotonic tension test was performed to determine the yield strength, the tensile strength, the percent of elongation and the percent reduction of area. Hardness tests were performed on the surface of three fatigue specimens using a Rockwell C scale. The hardness measurements were repeated three times for each specimen and the average value was recorded.

All fatigue tests were carried out in a laboratory environment at approximately 25 ^{o}C using an MTS servo-controlled closed loop electrohydraulic testing machine. A process control computer, controlled by FLEX software [1] was used to output constant strain and stress amplitudes in the form of a sinusoidal wave.

Axial, constant amplitude, fully reversed (R=-1) strain-controlled fatigue tests were performed on smooth specimens. The stress-strain limits for a given cycle of each specimen were recorded at logarithmic intervals throughout the test via a peak reading oscilloscope. Failure of a specimen was defined as a 50 percent drop in tensile peak load from the peak load observed at one half the expected specimen life. For fatigue lives greater than 100,000 reversals, the specimens were tested in stress-control once the stress-strain loops had stabilized. For the stress-controlled tests, failure was defined as the separation of the smooth specimen into two pieces. For strain-controlled tests the loading frequency varied from 0.03 Hz to 5 Hz while in stress-controlled tests the frequency used was up to 30 Hz.

The first reversal of each fatigue test was recorded on an x-y plotter, allowing the elastic modulus (E) and the monotonic yield strength to be determined.

RESULTS

A) Microstructural Data

Figure 2 presents the pearilitic-martensitic microstructure of AISI 1090M (GM) Hot Form-Accelerated Cooled steel. A type A inclusion rate of $1\frac{1}{2}$ was obtained based on the severity level number according to ASTM E45 method A. Inclusions of types B, C, and D were not observed. Figure 3 presents the observed inclusions of AISI 1090M (GM) Hot Form-Accelerated Cooled steel. The inclusion area was measured using a JAVA image analysis system. The volume fraction of pearlitic structure based on ASTM E562-95 and using the JAVA image analysis system was over 95%. The chemical composition of AISI 1090M (GM) Hot Form-Accelerated Cooled steel was provided by SCI-Lab materials testing inc., 25 McIntyre place, unit 2, Kitchener, Ontario, N2R 1H1, and is shown in Table 1.

B) Strain-Life Data

The fatigue test data for AISI 1090M-Accelerated Cooled steel obtained in this investigation are given in table 2. The stress amplitude corresponding to each strain-amplitude was calculated from the peak load amplitude at one half the expected specimen life.

A fatigue strain-life curve for the AISI 1090M-Accelerated Cooled steel is shown in Figure 4, and may is described by the following equation:

$$\frac{\Delta\varepsilon}{2} = \frac{\sigma'_f}{E}(2N_f)^b + \varepsilon'_f(2N_f)^c$$

where $\frac{\Delta\varepsilon}{2}$ = True total strain amplitude

$2N_f$ = Number of reversals to failure

σ'_f = Fatigue strength coefficient

b = Fatigue strength exponent

ε'_f = Fatigue ductility coefficient

c = Fatigue ductility exponent

Where σ'_f =1949.25 MPa, **b** = -0.1207, ε'_f = 0.8107 and **c** = -0.6430. These values of the strain-life parameters were determined from fatigue testing over the range: $0.002 < \frac{\Delta\varepsilon}{2} < 0.01$.

C) Cyclic Stress-Strain Curves

Stabilized and half life stress data obtained from strain-life fatigue tests were used to obtain the companion cyclic stress-strain curve shown in figure 5. The true cyclic stress-strain curve is described by the following equation:

ab8

$$\varepsilon = \frac{\sigma}{E} + \left(\frac{\sigma}{K'}\right)^{\frac{1}{n'}}$$

where ε = True total strain amplitude

σ = Cyclically stable true stress amplitude

K' = Cyclic strength coefficient

n' = Cyclic strain hardening exponent

Where $\mathbf{K'}$ = 1942.70 MPa and $\mathbf{n'}$ = 0.1794.

D) Mechanical Properties

The engineering monotonic stress-strain curve is given in figure 6. The monotonic and cyclic properties are included in Appendix 1. The Hardness of the AISI 1090M-Accelerated Cooled steel taken as the average of three randomly chosen fatigue specimens and is given in Appendix 1. The individual hardness measurements are also given in Table 2. The true monotonic and true cyclic stress-strain curves plotted together are given in figure 7.

REFERENCES

[1] Pompetzki, M.A., Saper, R.A., and Topper, T.H., "Software for High Frequency Control of Variable Amplitude Fatigue Tests," Canadian Metallurgical Quarterly, Vol. 25, No. 2, pp. 181-194, 198.

[2] J. A. Bannantine, J. J. Comer, and J. L. Handrock (1990), In :Fundamentals of Metal Fatigue Analysis, Prentice Hall, London.

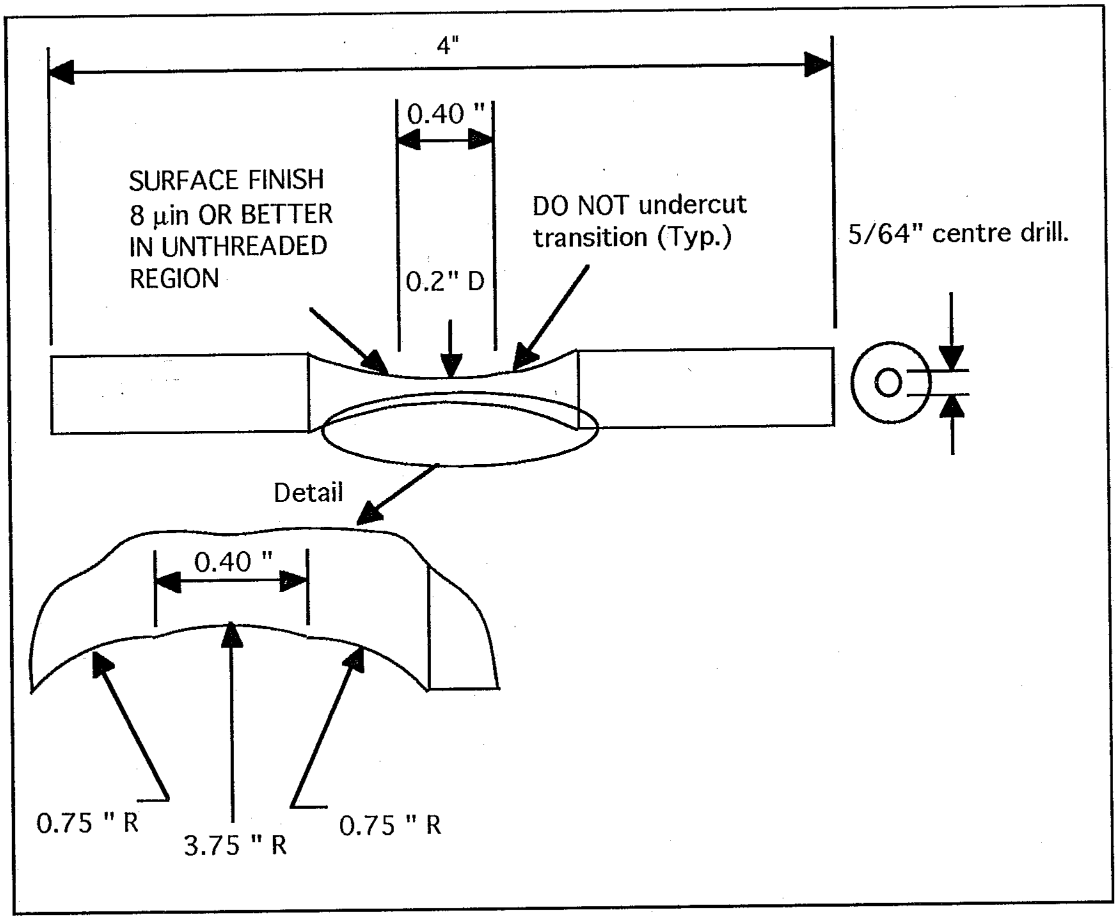
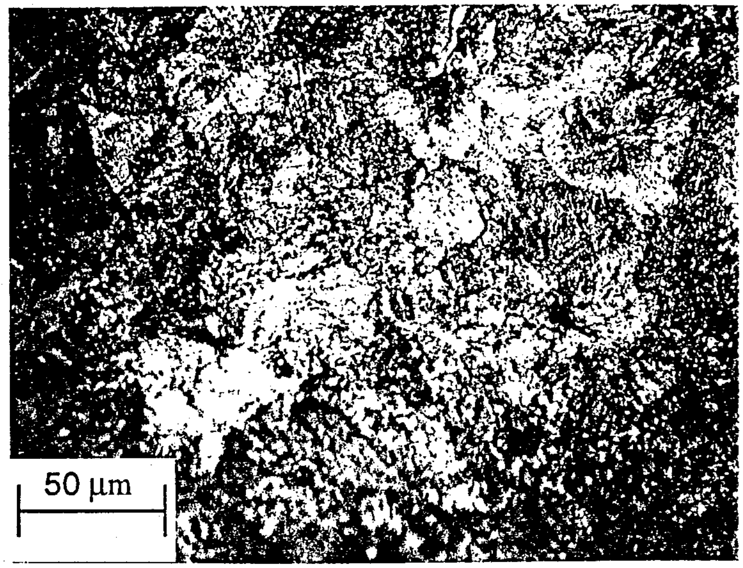
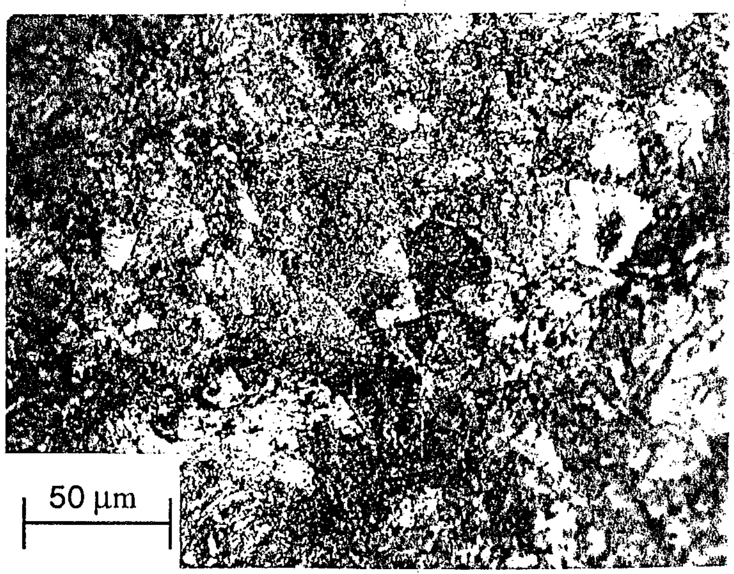


Fig. 1 Smooth cylindrical fatigue specimen



ITER 9: Photomicrograph of SAE 1090M steel, Hot Forged and Accelerated cooled to Rc-28. 500X Mag.

(a) Longitudinal direction



(b) Transverse direction

Fig. 2 Photomicrograohs of AISI 1090M-Accelerated Cooled steel (X500): (a) Longitudinal direction, and (b) Transverse direction.

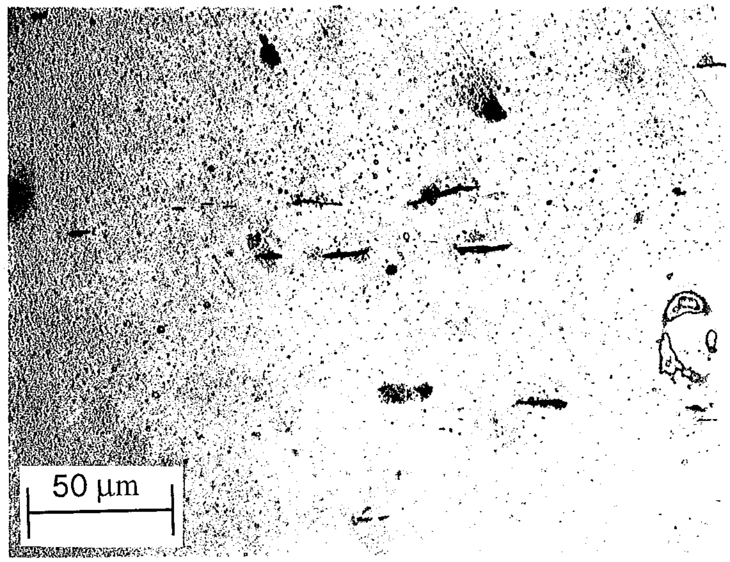


Fig. 3 Inclusions photomicrograoh of AISI 1090M (GM) Hot Form-Accelerated Cooled steel (X500)

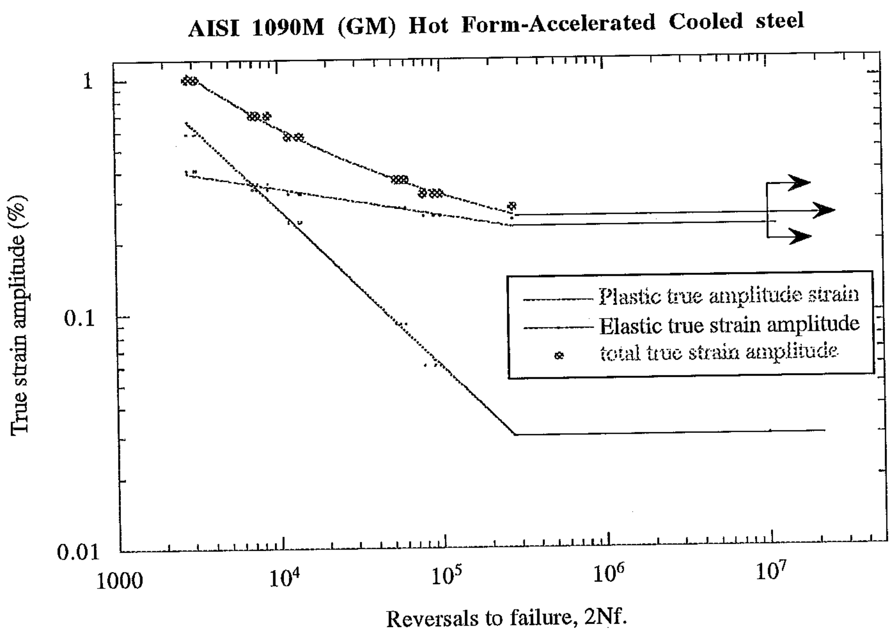


Fig. 4 Constant amplitude fully reversed strain-life curve for AISI 1090M (GM) Hot Form-Accelerated Cooled steel.

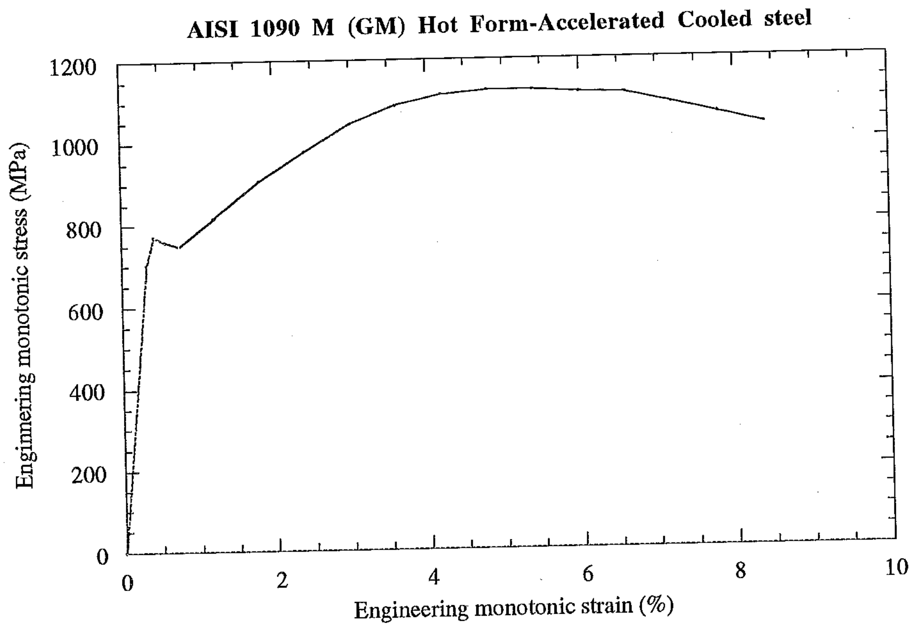


Fig. 5 Monotonic stress-strain curve for AISI 1090M (GM) Hot Form-Accelerated Cooled steel

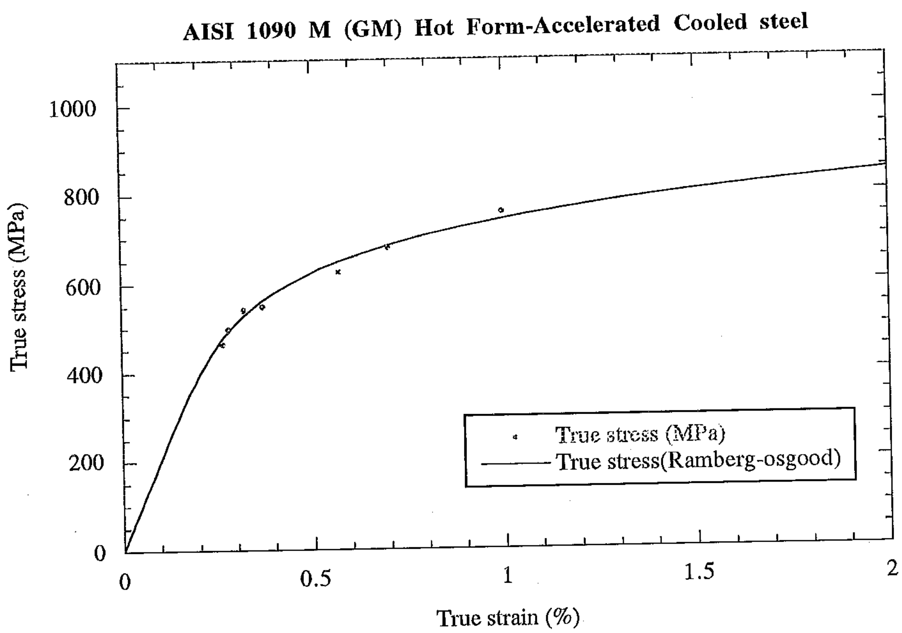


Fig. 6 Cyclic stress-strain curve for AISI 1090M (GM) Hot Form-Accelerated Cooled steel

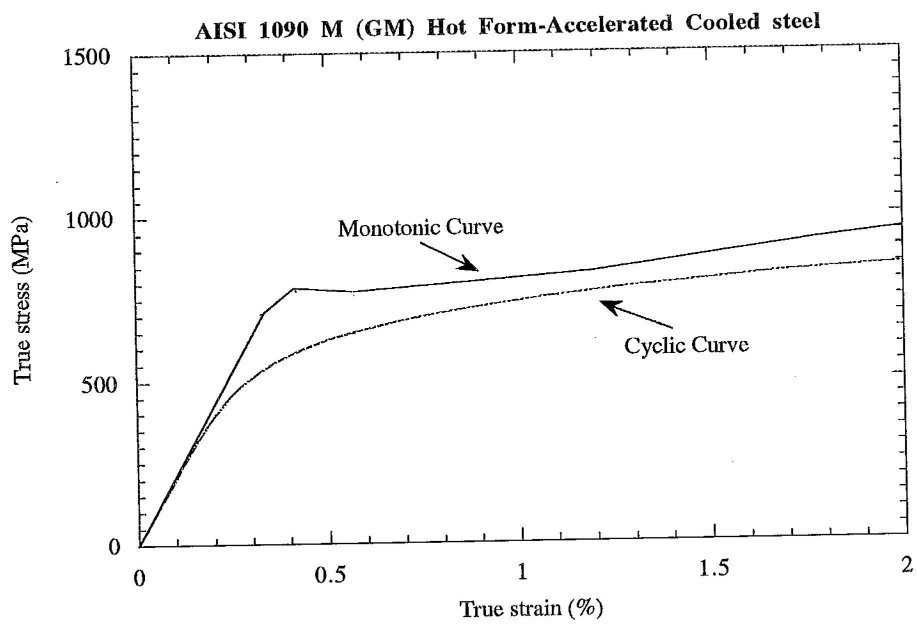


Fig. 7 Monotonic and Cyclic stress-strain curves for AISI 1090M (GM) Hot Form-Accelerated Cooled steel

Table 1 Chemical composition of AISI 1090M (GM) Hot Form-Accelerated Cooled steel

Carbon, C	0.88%
Manganese, Mn	0.58%
Phosphorous, P	0.002%
Sulfur, S	0.021%
Silicon, Si	0.22%
Copper, Cu	0.28%
Nickel, Ni	0.08%
Chromium, Cr	0.14%
Molybdenum, Mo	0.02%
Vanadium, Va	0.030%
Calcium, Ca	0.002%
Boron, Bo	0.0024%
Aluminum, Al	<0.001%
Titanium, Ti	0.001%
Oxygen, O	0.0024%
Columbium, Cb	0.003%

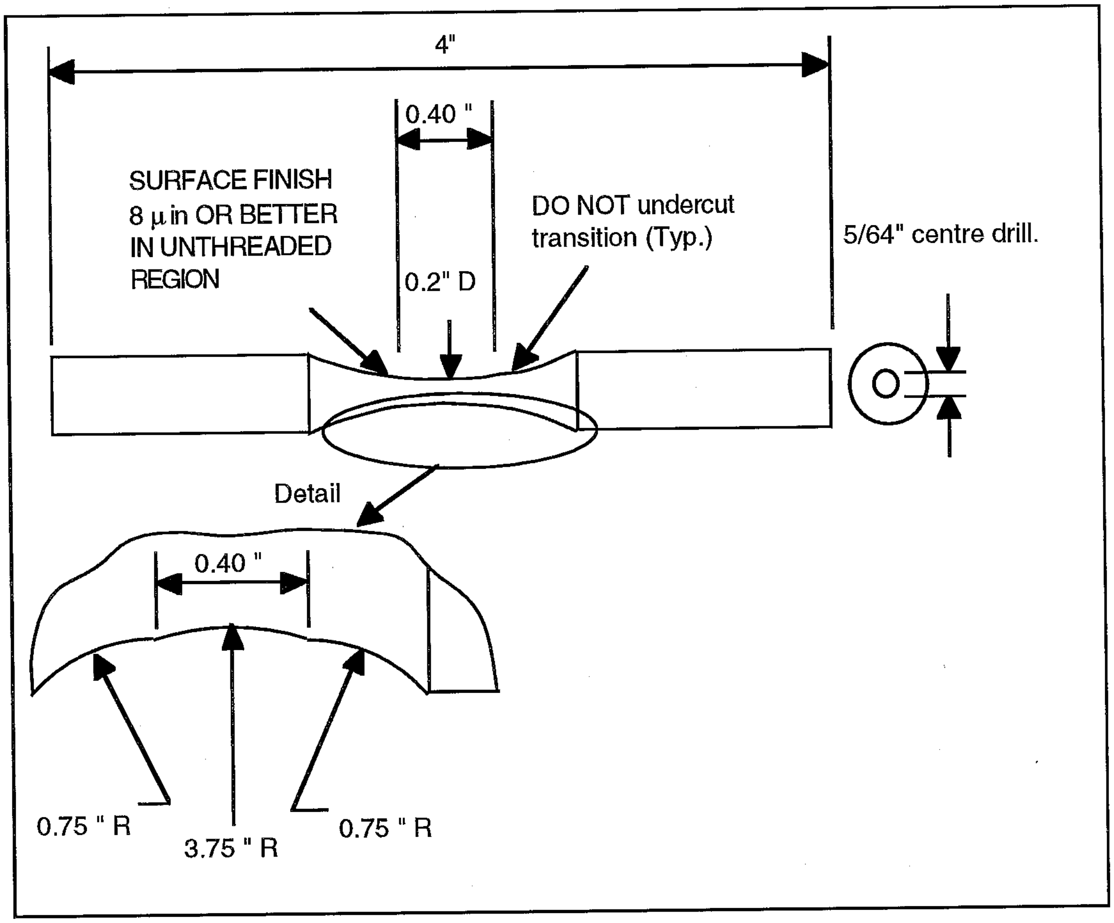


Fig. 1 Smooth cylindrical fatigue specimen

Table 2 Tensile and Fatigue Test Data for 1090M-Accelerated Cooled steel

Sp#	TRUE Total Strain Amplitude(%)	TRUE Stress Amplitude (MPa)	TRUE Plastic Strain Amplitude(%)	TRUE Elastic Strain Amplitude(%)	(50% load drop) Fatigue Life (Reversals, 2Nf)	MONOTONIC Young's Modulus(GPa)	Hardness (HRC)
GM18	0.995	807.23	0.621	0.376	2138	219.50	29
GM27	0.995	847.92	0.602	0.395	1254	219.50	
GM23	0.995	802.95	0.623	0.374	1284	219.50	
GM19	0.697	695.96	0.373	0.325	5192	191.50	29
GM8	0.697	706.63	0.368	0.330	6020	191.50	29
GM12	0.697	715.17	0.364	0.334	5756	191.50	
GM11	0.568	673.74	0.253	0.315	8840	219.50	
GM3	0.568	652.42	0.263	0.305	8780	219.50	
GM16	0.568	641.76	0.268	0.300	9506	219.50	29
GM26	0.319	508.30	0.080	0.238	50738	219.50	
GM28	0.319	531.70	0.069	0.249	47666	219.50	
GM5	0.319	508.30	0.080	0.238	44950	219.54	
GM29	0.279	488.97	0.049	0.229	44366	219.50	
GM13	0.279	467.71	0.059	0.219	70228	219.50	29
GM21	0.279	495.34	0.046	0.232	97556	219.50	
GM20	0.224	450.47	0.017	0.211	408300	200.00	
GM21	0.219	424.93	0.019	0.199	10000000*	206.85	
GM8	0.219	427.06	0.018	0.200	10000000*	206.85	
GM30	0.219	429.18	0.017	0.201	10000000*	206.85	29

* Run out

8/6/98

Appendix 1

Monotonic Properties for AISI 1090M-Accelerated Cooled steel

Average Elastic Modulus, E	=	212 GPa
Upper Yield Strength	=	768.30 MPa
Lower Yield Strength	=	751.30 MPa
Ultimate tensile Strength	=	1251.25 MPa
% Elongation	=	6.66 %
% Reduction of Area	=	13.56 %
True fracture strain, $Ln\ (A_i / A_f)$	=	14.6 %
True fracture stress, $\sigma_f = \frac{P_f}{A_f}$	=	1422 MPa
Bridgman correction, $\sigma_f = \frac{P_f}{A_f} \Big/ \left(1+\frac{4R}{D_f}\right) Ln\left(1+\frac{D_f}{4R}\right)$	=	1169 MPa
Monotonic strength coefficient, K	=	2273.3 MPa
Monotonic strain hardening exponent, n	=	0.1934
Hardness, Rockwell C (HRC)	=	29 HRC
Hardness, Brinell	=	279

Cyclic Properties for AISI 1090M-Accelerated Cooled steel

Cyclic Yield Strength, (0.2% offset) $= K'(0.002)^{n'}$	=	637 MPa
Cyclic strength coefficient, K'	=	1942.70 MPa
Cyclic strain hardening exponent, n'	=	0.1794
Fatigue Strength Coefficient, σ'_f	=	1949.25MPa
Fatigue Strength Exponent, b	=	-0.1207
Fatigue Ductility Coefficient, ε'_f	=	0.8107
Fatigue Ductility Exponent, c	=	-0.6430

P_f:	Load at fracture.
A_i and A_f:	Specimen cross-section area before and after fracture.
R:	Specimen neck radius.
D_f	Specimen diameter at fracture.

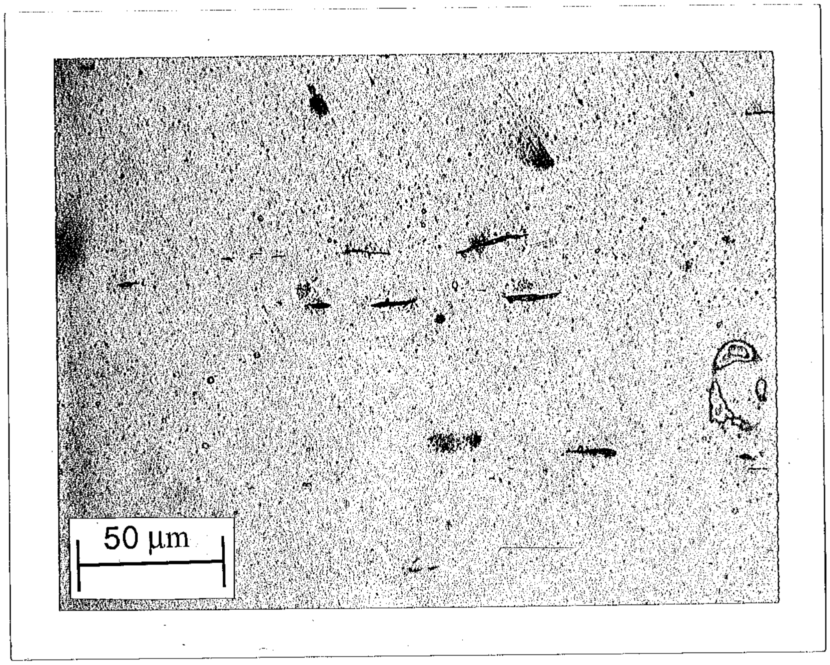


Fig. 3 Inclusions photomicrograoh of AISI 1090M (GM) Hot Form-Accelerated Cooled steel (X500)

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1090M
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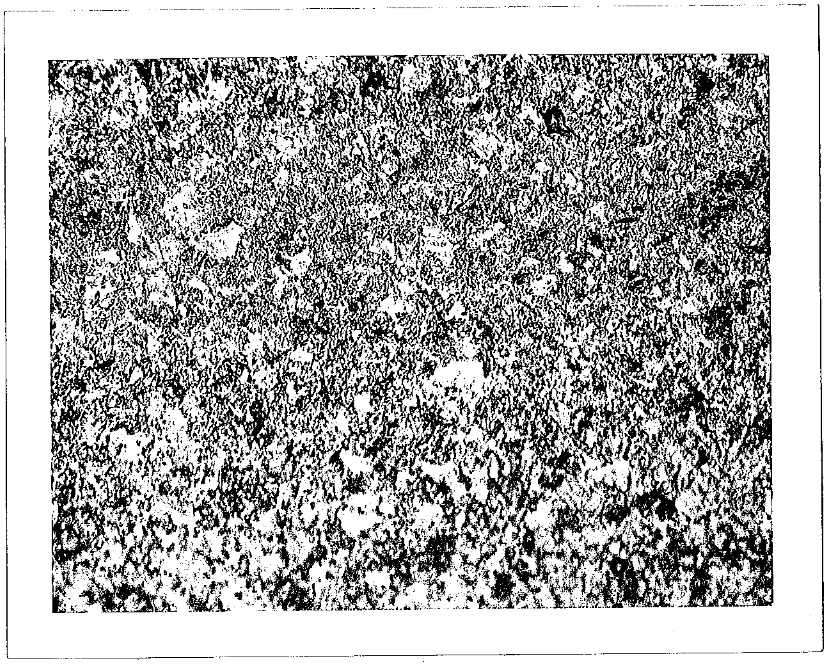
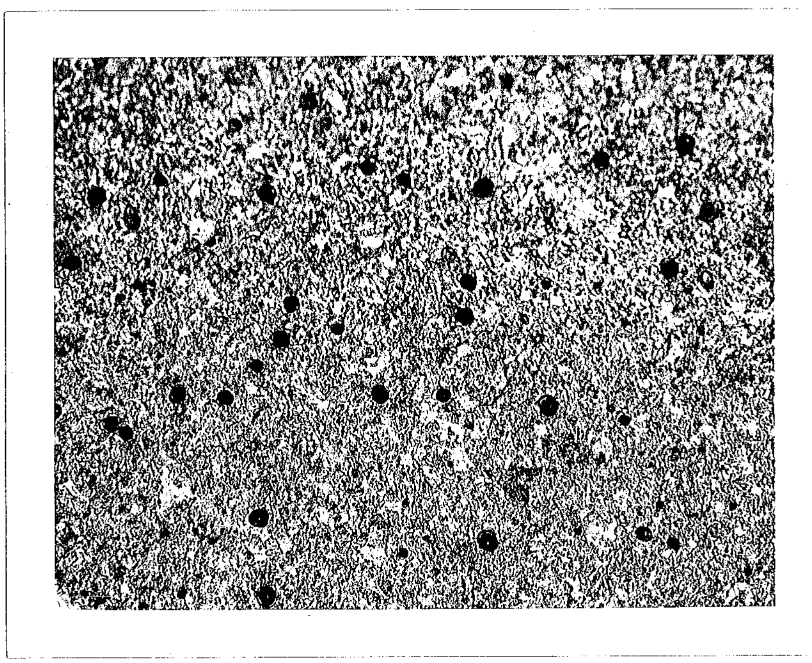


(a) Longitudinal direction



(b) Transverse direction

Fig. 2 Photomicrograohs of AISI 1090M (GM) Hot Form-Accelerated Cooled steel (X200):
(a) Longitudinal direction, and (b) Transverse direction.

AISI Bar Application Group Fatigue Project
Test Matrix (6-9-98)

Iter. No.	Steel	Supplier	Status	Part Fabrication	Fabricated Hdns	Microstructure	School	Bar or Part
1	1541	RES	Complete 2-4-98	Normalize 1650F		Ferrite/Pearlite	Waterloo	HR Bar
2	1541	RES	Complete 2-4-98	Cold Size/Form	Rb 85 min.	Ferrite/Pearlite	Waterloo	HR Bar
3	1050M	Stelco	Complete 7-30-97	Normalize 1650F		Ferrite/Pearlite	Waterloo	Hr Bar
4	1050M	Chrysler	Complete 6-9-98	Hot Forge, Cold Extrude (Core)	Rc 35 max.	Martensite	Waterloo	Axles
5	1050M	Chrysler	Complete 6-9-98	Induction Surface Hardened (Case)	Rc 58 min.	Martensite	Waterloo	Axles
6	1090	NS	Complete 6-9-98	Normalize 1650F		Pearlite	Waterloo	Hr Bar
7	1090M	Chrysler	Complete 6-9-98	Hot Form + Acc. Cool	BHN 341-444	Martensite/Bainite	Waterloo	Stab Bar
8	1090	Chrysler	Complete 2-4-98	Hot Form + Q&T	BHN 341-444	Martensite	Waterloo	Stab Bar
9*	1090M	GM/AMM	Complete 2-4-98	Hot Form + Acc. Cool	BHN 302-363	Martensite/Bainite	Waterloo	Stab Bar
10*	1090	GM/Mather	Complete 6-9-98	Hot Form + Austemper	BHN 3.0-3.5	Bainite	Waterloo	Stab Bar
11	1141(AlFG)	RES	Complete 6-9-98	Normalize 1650F		Ferrite/Pearlite	Toledo	Hr Bar
12	1141(AlFG)	RES	Complete 6-9-98	Reheat, Q&T	BHN 229-269	Martensite	Toledo	Hr Bar
13	1141(NbFG)	NS	Complete 6-9/98	Normalize 1650F		Ferrite/Pearlite	Toledo	Hr Bar
14	1141(NbFG)	NS	Complete 6-9-98	Reheat, Q&T	BHN 229-269	Martensite	Toledo	Hr Bar
15	1141(VFG)	NS	@Toledo	Normalize 1650F		Ferrite/Pearlite	Toledo	Hr Bar
16	1141(VFG)	NS	@Toledo	Reheat, Q&T	BHN 229-269	Martensite	Toledo	Hr Bar
17	1141(VFG)	NS	@Toledo	Normalize @ High Temp (1750F)	TBD	Ferrite/Pearlite	Toledo	Hr Bar
18	1038	Stelco	Complete 10-9-97	Normalize 1650F		Ferrite/Pearlite	Toledo	Hr Bar
19	1038	Stelco	Complete 6-9-98	Cold Size/Form	Rb 85 min.	Ferrite/Pearlite	Toledo	Hr Bar
20	1038	Stelco	@Toledo-Re-H.T.	Reheat, Q&T, (Temper @ 930F)	Rc 20-30	Martensite	Toledo	Hr Bar
21	10V45	Inland	@Toledo	Normalized 1650F		Ferrite/Pearlite	Toledo	Hr Bar
22	10V45	Inland	@Toledo	Reheat, 2250F, Deform @ 2000F, FAC	RC 25-30	Ferrite/Pearlite	Toledo	Hr Bar

*These iterations will be supplied by GM, and funded separately from the rest of the program.