

## Results for eg.ifpipeout2.0 : Crack Propagation Int. Pipe Surface Flaw

Author: edit file makereport3 to change

Affiliation:

Wed Jul 1 17:34:55 EDT 2020

Simulation input data:

**B**= 10.0 mm

**r<sub>i</sub>**= 50. mm

**a<sub>0</sub>**= 0.5 mm

**c<sub>0</sub>**= 4.0 mm

#MATERIAL= merged\_a36\_fitted.html

**K<sub>t</sub>**= 2.0

#TYPE= pipe\_inside\_surface\_flaw

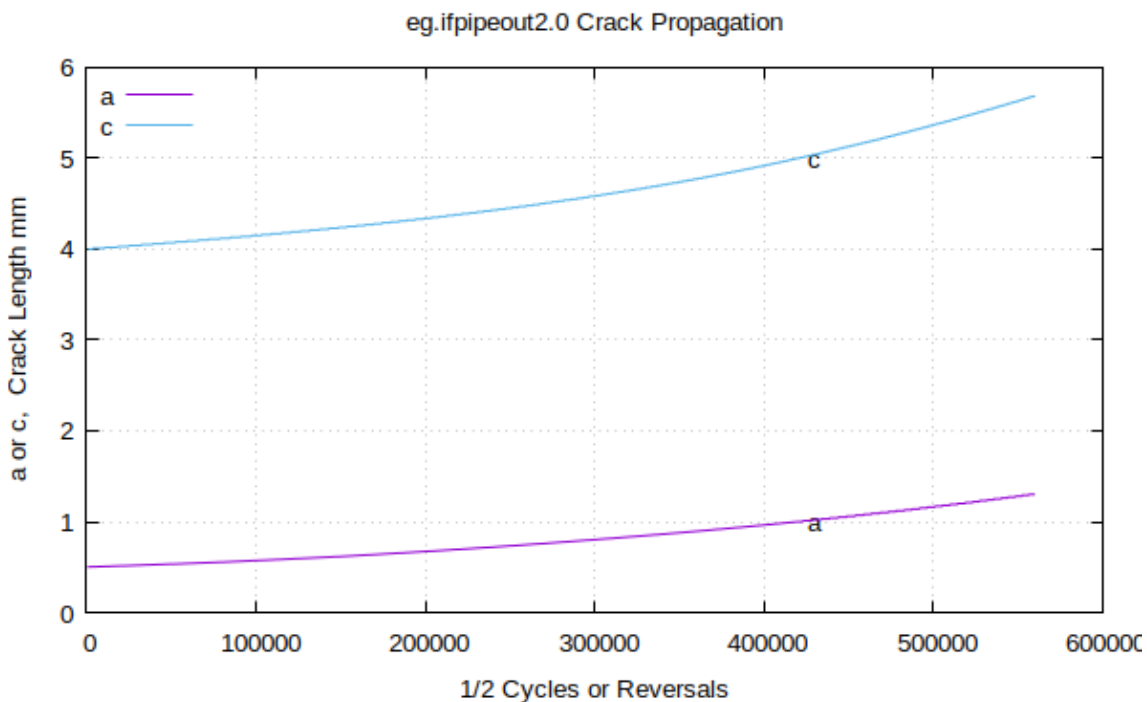
#ACTIVATE\_MmMb= 1 \_\_\_\_\_#ACTIVATE\_MkmMkb= 0 \_\_\_\_\_#ACTIVATE\_fw= 0

#Kmat= 1675.

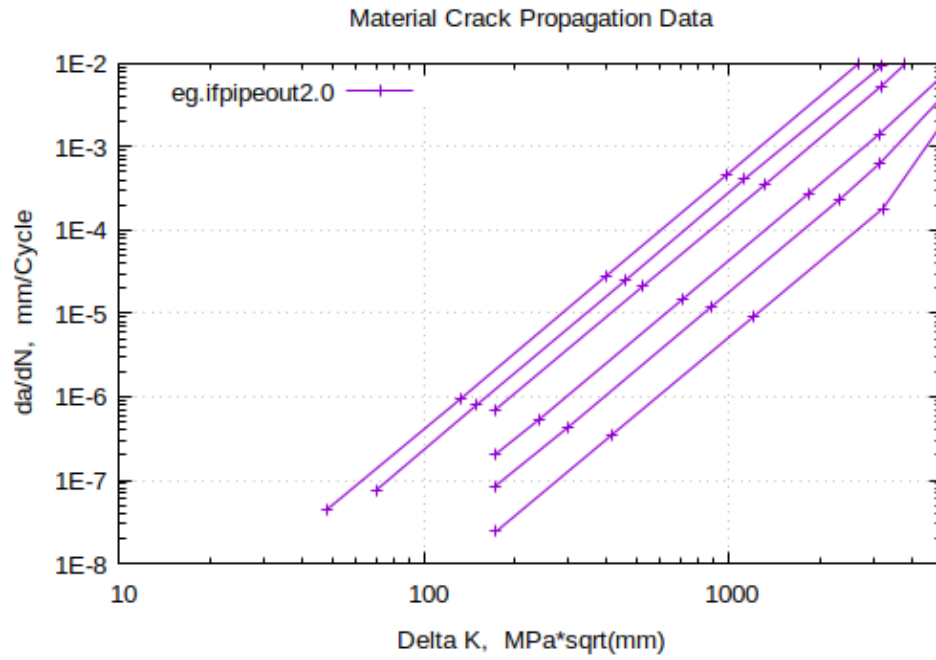
Crack Propagation Results:

( # pipeIntSurfFlaw.f vers. 5.2 June2020 # makereport3 vers. 2.6

- No. of Reversals= 560001 revs. or 280000 cycles
- Final \_\_\_\_\_ **a** = 0.130E+01 mm
- Final \_\_\_\_\_ **c** = 0.569E+01 mm
- No. of History Reps.= 40001 reps. + 1 revs.
- No. records = 840051 in random access data file



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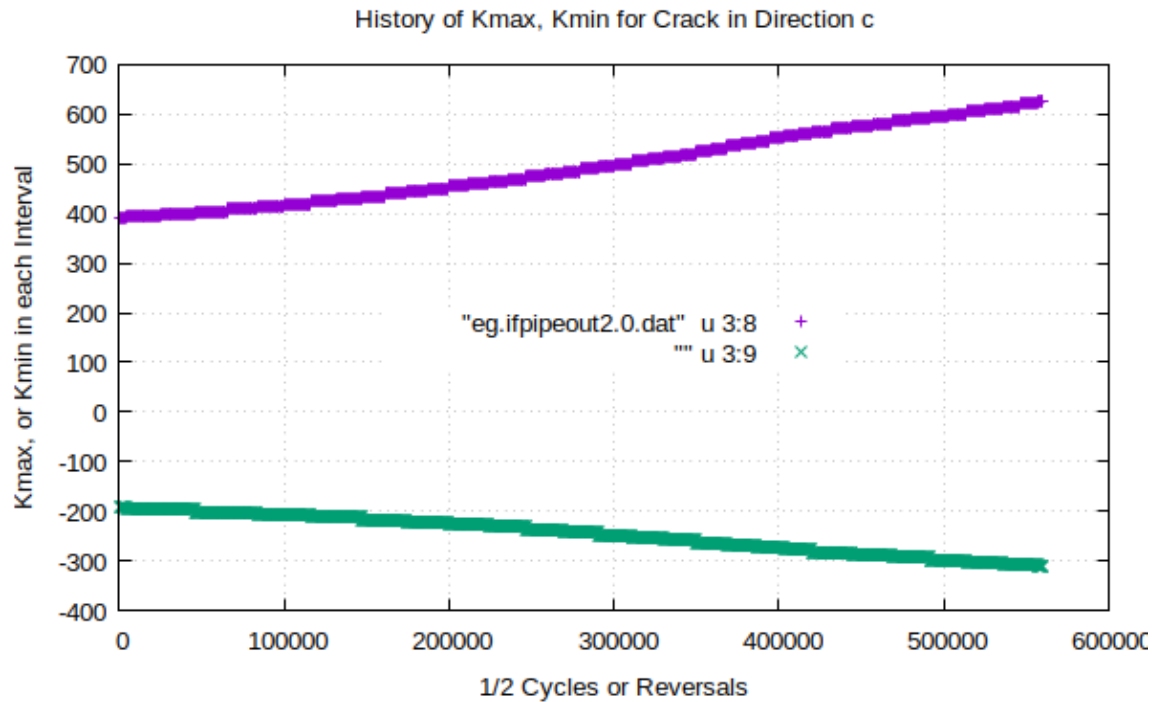
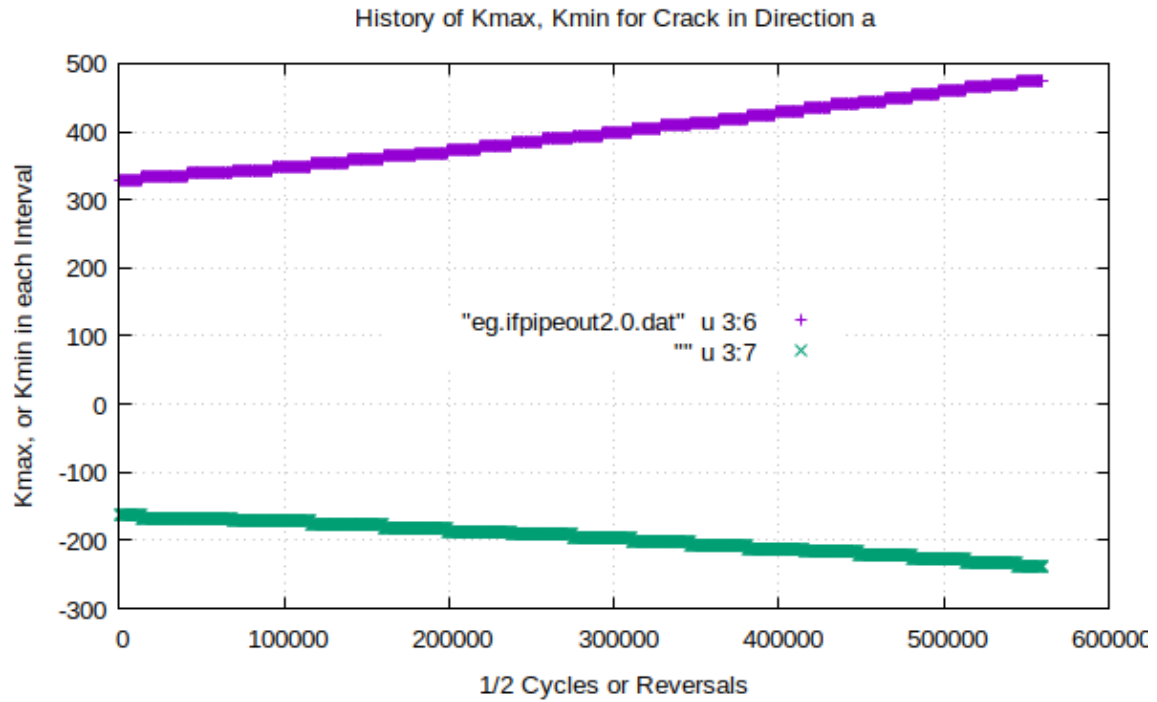


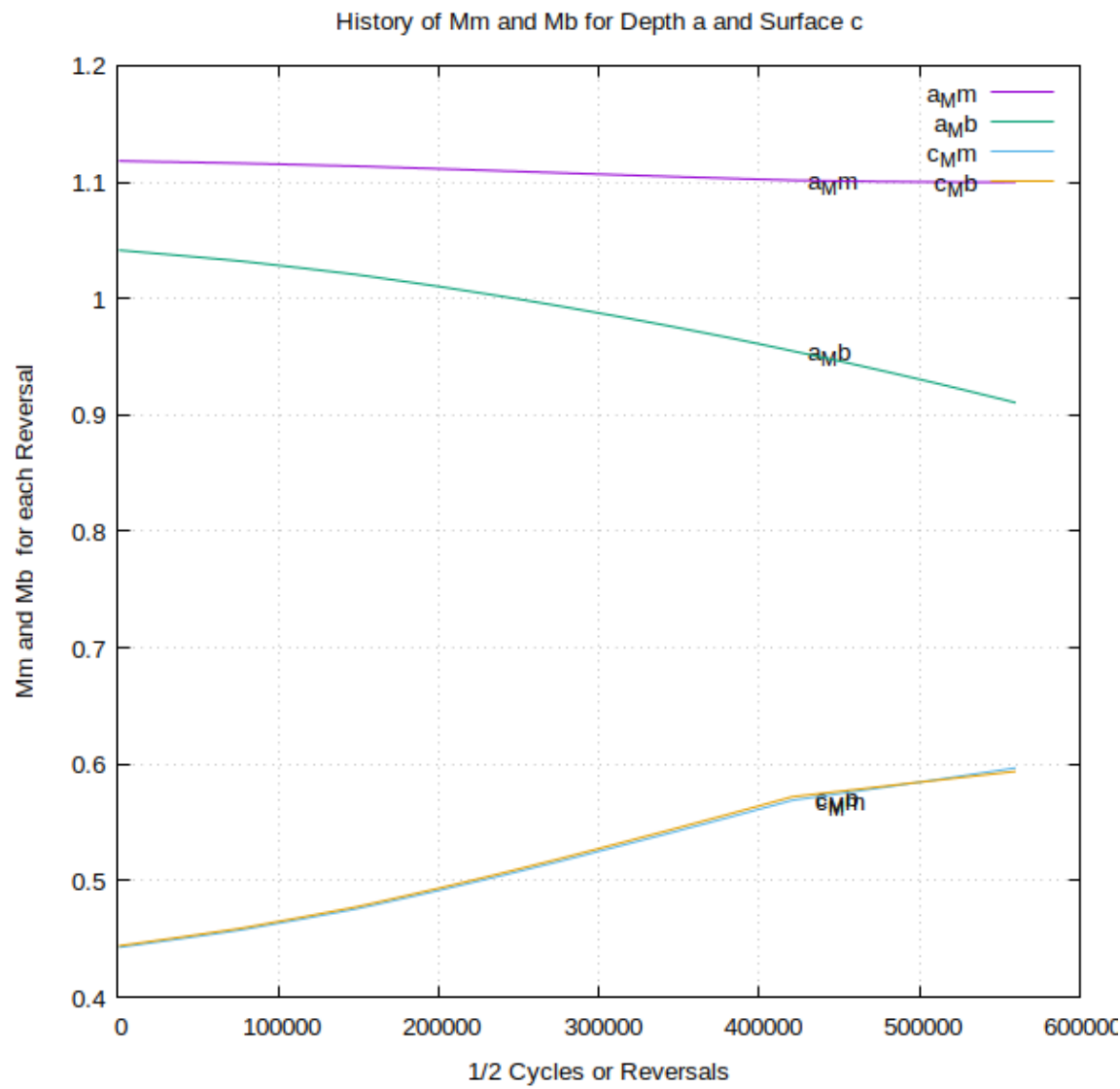
## Results for eg.ifpipeout2.0 : Crack Propagation Int. Pipe Surface Flaw

#DADN= ASME1994 # Can be "table" or "Paris" "USER" BS7910

#DADN\_PARIS= 0. 0. 0. 0. mpa\_mm

#DADN\_TABLE= none # da/dN digitized da/dN curve for material,





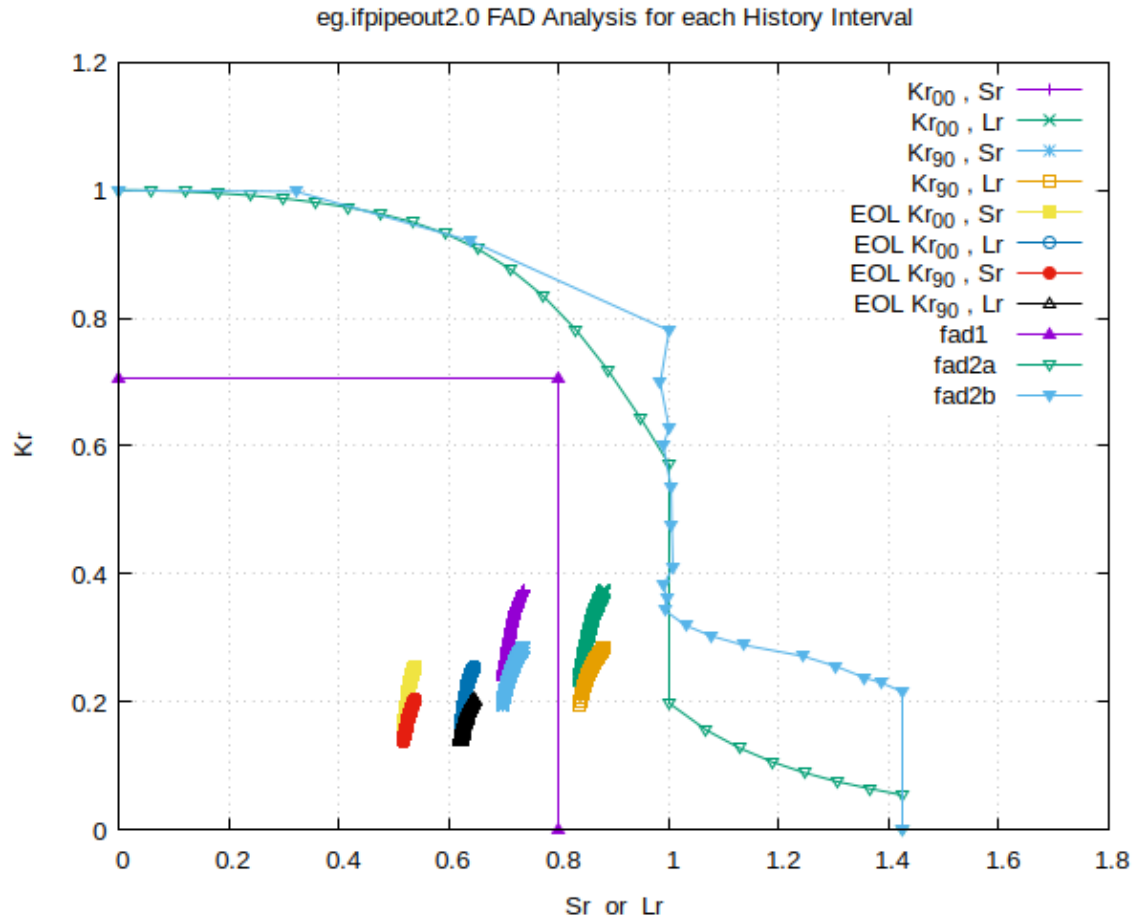
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## FAD Results for eg.ifpipeout2.0

#TensileFile= a36\_Mattos\_mono\_engrSS\_FLAT.txt

#PmEOL= 70. #PbEOL= 100.

#Kmat= 1675.



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## Crack Initiation Life Results for eg.ifpipeout2.0 (Using $K_t = 2.0$ )

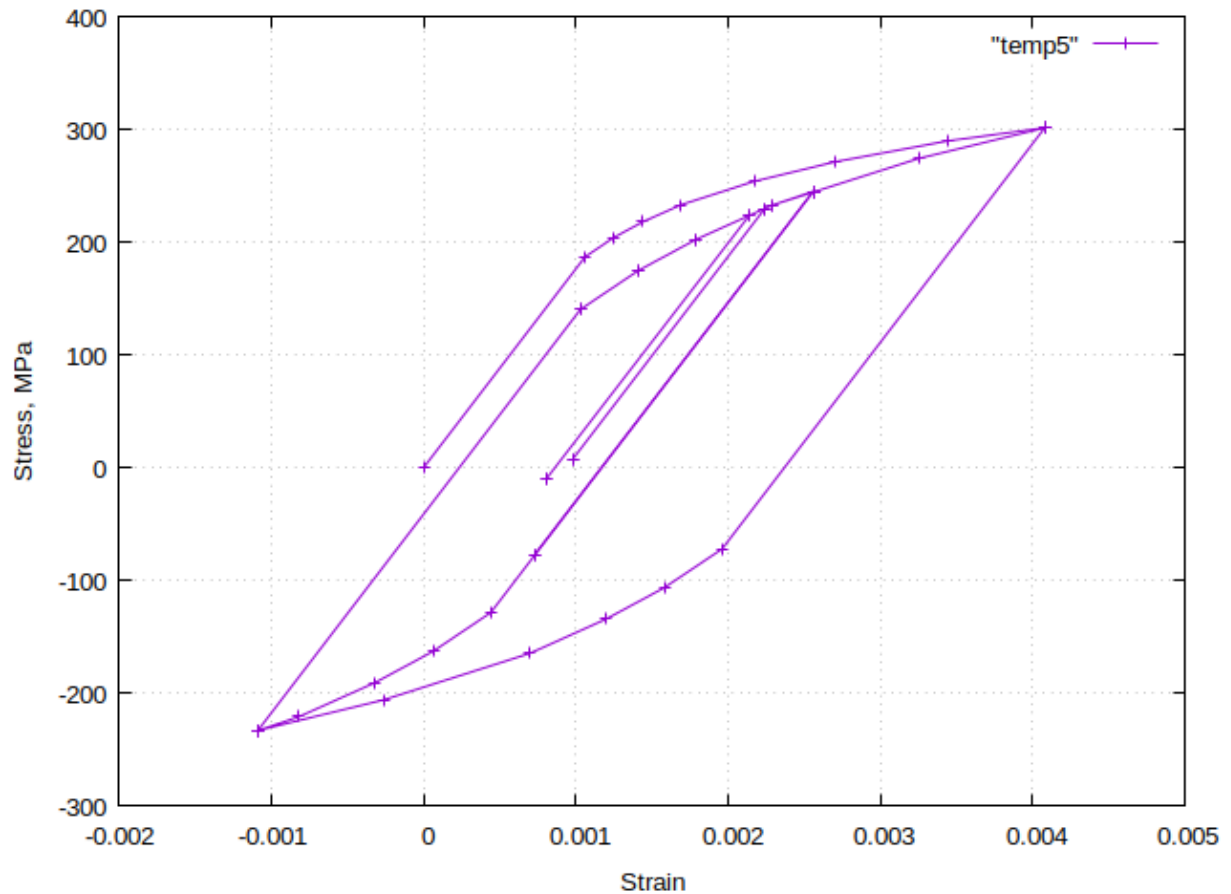
Files Used:

- Stress History (Sb+Sm)
- Rainflow File
- Material File

Predicted History Repetitions to Initiation:

StrainLife_Reps	SWT_Life_Reps	StressLife_Reps	Morrow_Reps	Goodman_Reps	(Reps= Repetitions)
44105.2	34187.0	44105.3	30154.8	22551.4	

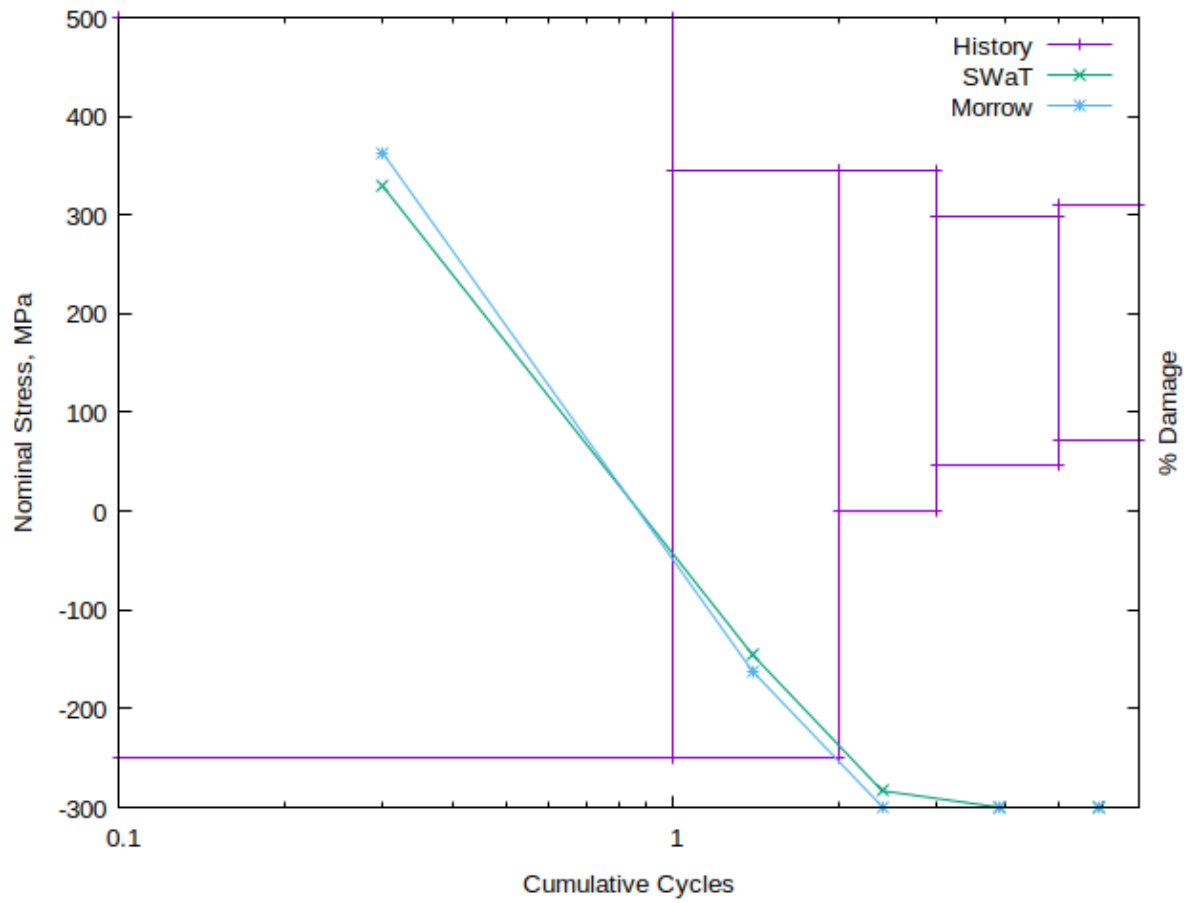
### Local Stress and Strain Response:





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## Cumulative Cycle Plot of History and Damage:



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(Rectangles are Rainflow Cycle Sets: Sorted by Range: largest on Left)

### Detailed Damage for each Rainflow Cycle Set:

Loop	Smax	Smin	N	Sigmax	Sigmin	Delta	Epsmax	Epsmin	DeltaEps	%Eps	%SWT	%St
1	500.0	-250.0	1.0	301.	-233.	535.	0.00408	-.00109	0.00517	76.7	78.6	76.7
2	346.0	-250.0	1.0	245.	-233.	478.	0.00256	-.00109	0.00365	23.3	19.3	23.3
3	346.0	0.0	1.0	245.	-77.	322.	0.00256	0.00073	0.00183	0.0	2.1	0.0
4	298.0	47.6	2.0	224.	-9.	233.	0.00214	0.00081	0.00132	0.0	0.0	0.0
5	310.0	71.4	2.0	230.	8.	222.	0.00224	0.00098	0.00126	0.0	0.0	0.0

## Appendix 1: Print of "pdprop.env" Simulation Control file

```
# Vers. 5.0 Jul 2020 Allows multiple dadn files/curves.

# This file contains the starting filenames, variables etc
# for the Crack Propagation programs. It should be edited by the
# user before each simulation run. It can also be generated from web
# page at: to be determined
#

#TYPE= pipe_inside_surface_flaw #with or without weld using ACTIVATES:
#ACTIVATE_MmMb= 1 # Deactivate = 0
#ACTIVATE_MkmMkb= 0 # Set to off for inside surf. flaw.( not available )
#ACTIVATE_fw= 0 # Set to off for inside surf. flaw.( fw=1.0 )

# #Other #TYPE= options:
# # plate_surface_flaw
# # plate_long_surface_flaw
# # plate_tru_flaw
# # plate_embedded_flaw
# # plate_edge_flaw
# #
# # pipe_inside_surface_flaw
# # pipe_long_inside_surface_flaw
# # pipe_full_inside_flaw
# # pipe_full_outside_flaw
# #
# # rod_surface_flaw
# # rod_full_outside_flaw

# # These problem types are used to pull in the
# # appropriate Fw, Mm, Mb, files etc.

# The factors described in this section may be ignored if not applicable to
# the particular problem type described above.
# (All dimensions in mm)
#B= 10.0 # plate (or pipe wall) thickness
#W= 0.0 # plate width
#ri= 50. # Internal diameter if pipe problem
#azero= 0.5 # initial crack depth
#czero= 4.0 # initial 1/2 crack width at surface
#L= 0. # Weld Feature width. Set to 0.0 if no Mkm or Mkb (weld)

#HISTORYFILE= load1.txt # historyFileName
# # Adjustments to load file variables:
# # Note that the MEANADD (below) is added AFTER the MAGFACTOR is applied.
#MAGFACTOR_m= 1.0 # Multiply factor on membrane load. Result should be MPa
#MAGFACTOR_b= 1.0 # Multiply factor on bending load term. Result should be MPa
#MEANADD_m= 0.0 # Mean shift in MPa added to membrane stress.
```

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```
#MEANADD_b= 0.0      # Mean shift in MPa added to bending stress.

#MAXREPS= 40000      # Max no. history repeats in simulation.
#                   # One repetition or application of the load history is
#                   # also called a "block" of cycles.
#                   # Normally this would be some large number.
#
#MATERIAL= merged_a36_fitted.html  #File name of material fitted data
#                                   This file is used to define the cyclic
#                                   stress-strain curve, and the Neuber Product curve.
#Kt= 2.0                    # Ktg gross. The history is in gross stress for cracks.
#                           #Stress Conc. Factor, presently for crack init. calcs only
#
#DADN= ASME1994             # Can be "table" or "Paris" "USER" BS7910
#                           # HASEGAWA2019, HASEGAWA2016 or ASME1994
#                           # If "table" only one dadn file is expected
#                           # and it is specified by #DADN_TABLE= filename below.
#                           # If "USER" copy your prepared dadn files into
#                           # filenames: dadnTable01, dadnTable02, dadnTable03, etc.
#
#DADNFileNum= 1             # With "USER" only: no. of dadn files or curves
#                           # (ignored if NOT "USER" above.)
#                           # Run "setup1" when changing this.
#
#DADN_PARIS= 0.  0.  0.  0.  mpa_mm      units      (ignored if #DADN not Paris )
#           # Kth  a   m   Kc             !! specify:  mpa_m   or  ksi_in  or  mpa_mm
#                                           ksi_in: ksi stress, inch crack length, inches in delta_K
#                                           mpa_m:  mpa stress,   m crack length, meters in delta_K
#                                           mpa_mm: mpa stress,   mm crack length, mm in delta_K
#                                           same as N/(mm**(3/2))
#DADN_TABLE= none          # da/dN digitized da/dN curve for material,
#                           including the threshold, and KIc.
#                           If a threshold exists, put in a vertical line
#                           (with two identical X-axis points).
#                           If the threshold needs to be "turned off" then
#                           do NOT put in a vertical line at low da/dN.
#                           (Ignored when #DADN= not table )
#
#FAD Stuff:
#TensileFile= a36_Mattos_mono_engrSS_FLAT.txt      #enter "none" if no FAD
#PmEOL= 70.                    #Set these so that Pm+Pb= 0.82*Syield for default.
#PbEOL= 100.
#Kmat= 1675.                   # KIc See BS7910 Sec. 7.1.5 for details. Used for Fracture.
#PinJoint= 0                   #Set = 1 if struture is pinJointed (for bending)
#
#BLOCKSKIP= 1.0 percent       # At the end of each block check if the previous
#                               two blocks of cycles had similar damage (crack
#                               extension) within this percentage. If TRUE then
#                               simply skip the simulation of the next block,
#                               but just add the expected damage. Continue by
#                               simulating the block after the skip.
#                               A value of 0.0 will disallow skipping blocks.
#SAVELEVEL= 0                 #Amount of output saved to disk:
#                               # 3=lots 2=medium 1=minimal
#                               # 0= save #crk= data into binary direct access file only
#                               # No #crk= data will be written into the text logfile.
#                               # Use for large output files with lots of cycles.
```

## Appendix 2: Print of da/dn vs DeltaK Table in file eg.ifpipeout2.0

Delta_K	da/dn						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	1 R= -2.00						
0.1729261E+03 0.2404800E-07 0.2237861E+01 -0.7618921E+01 0.0000000E+00	0.0000000E+00						
0.4135313E+03 0.3444500E-06 0.2616508E+01 -0.6462874E+01 0.3786478E+00	0.1156047E+01						
0.1214695E+04 0.9184000E-05 0.3084467E+01 -0.5036968E+01 0.4679587E+00	0.1425906E+01						
0.3233779E+04 0.1829500E-03 0.3509710E+01 -0.3737668E+01 0.4252431E+00	0.1299301E+01						
0.1010100E+05 0.6410000E-02 0.4004364E+01 -0.2193142E+01 0.4946542E+00	0.1544526E+01						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	2 R= -1.00						
0.1720000E+03 0.8473000E-07 0.2235528E+01 -0.7071963E+01 0.0000000E+00	0.0000000E+00						
0.2997083E+03 0.4375100E-06 0.2476699E+01 -0.6359012E+01 0.2411704E+00	0.7129507E+00						
0.8843000E+03 0.1212200E-04 0.2946600E+01 -0.4916426E+01 0.4699008E+00	0.1442586E+01						
0.2322853E+04 0.2323800E-03 0.3366022E+01 -0.3633801E+01 0.4194219E+00	0.1282624E+01						
0.3162280E+04 0.6400000E-03 0.3500000E+01 -0.3193820E+01 0.1339786E+00	0.4399812E+00						
0.7071491E+04 0.7335000E-02 0.3849511E+01 -0.2134600E+01 0.3495107E+00	0.1059220E+01						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	3 R= -0.50						
0.1720000E+03 0.2033500E-06 0.2235528E+01 -0.6691756E+01 0.0000000E+00	0.0000000E+00						
0.2396692E+03 0.5346000E-06 0.2379612E+01 -0.6271971E+01 0.1440837E+00	0.4197845E+00						
0.7103113E+03 0.1492500E-04 0.2851449E+01 -0.4826086E+01 0.4718366E+00	0.1445886E+01						
0.1840985E+04 0.2753700E-03 0.3265050E+01 -0.3560083E+01 0.4136014E+00	0.1266002E+01						
0.3134136E+04 0.1411000E-02 0.3496118E+01 -0.2850473E+01 0.2310677E+00	0.7096105E+00						
0.5505213E+04 0.8238000E-02 0.3740774E+01 -0.2084178E+01 0.2446563E+00	0.7662947E+00						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	4 R= 0.00						
0.1720000E+03 0.7002000E-06 0.2235528E+01 -0.6154778E+01 0.0000000E+00	0.0000000E+00						
0.5241163E+03 0.2110800E-04 0.2719428E+01 -0.4675553E+01 0.4838991E+00	0.1479225E+01						
0.1328316E+04 0.3579200E-03 0.3123302E+01 -0.3446214E+01 0.4038739E+00	0.1229339E+01						
0.3190677E+04 0.5368300E-02 0.3503883E+01 -0.2270163E+01 0.3805814E+00	0.1176051E+01						
0.3798531E+04 0.9690000E-02 0.3579616E+01 -0.2013676E+01 0.7573271E-01	0.2564871E+00						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	5 R= 0.50						
0.7000000E+02 0.7633000E-07 0.1845098E+01 -0.7117305E+01 0.0000000E+00	0.0000000E+00						
0.1485418E+03 0.7861000E-06 0.2171849E+01 -0.6104522E+01 0.3267508E+00	0.1012783E+01						
0.4583093E+03 0.2462300E-04 0.2661159E+01 -0.4608659E+01 0.4893098E+00	0.1495863E+01						
0.1130831E+04 0.4080500E-03 0.3053398E+01 -0.3389287E+01 0.3922391E+00	0.1219373E+01						
0.3219359E+04 0.9476000E-02 0.3507769E+01 -0.2023375E+01 0.4543717E+00	0.1365911E+01						
#deltK dadn logdeltaK logdadn logdiffdk logdiffdadn File=	6 R= 0.90						
0.4835759E+02 0.4498600E-07 0.1684465E+01 -0.7346923E+01 0.0000000E+00	0.0000000E+00						
0.1316489E+03 0.9312000E-06 0.2119417E+01 -0.6030957E+01 0.4349525E+00	0.1315966E+01						
0.3989849E+03 0.2850500E-04 0.2600956E+01 -0.4545079E+01 0.4815392E+00	0.1485878E+01						
0.9888766E+03 0.4616100E-03 0.2995142E+01 -0.3335725E+01 0.3941855E+00	0.1209354E+01						
0.2680127E+04 0.9929000E-02 0.3428155E+01 -0.2003094E+01 0.4330134E+00	0.1332630E+01						

## Appendix 3: Print of Stress-Strain-Init.Life file: "matfile"

#SAE Standard Fatigue Data File format

##

Pick one: #FDE\_plot #FDE\_fit ##

## Results for eg.ifpipeout2.0 : Crack Propagation Int. Pipe Surface Flaw

```
#
#Copyright (C) 2012 F.D.E. Committee
#This data file is free software - you can redistribute it and/or
#modify it under the terms of the GNU General Public License as
#published by the Free Software Foundation; either version 2 of the
#license, or (at your option) any later version.
#This data file is distributed in the hope that it will be useful,
#but WITHOUT ANY WARRANTY - without even the implied warranty of
#MERCHANTABILITY or FITNESS FOR A PARTICULAR PURPOSE. See the
#GNU General Public License for more details.
#You should have received a copy of the GNU General Public License
#along with this program - if not, write to the Free Software
#Foundation, Inc., 59 Temple Place - Suite 330, Boston, MA 02111-1307, USA
#Try also their web site: http://www.gnu.org/copyleft/gpl.html
#
# NOTE: Fitted Data !!
# A36 Steel Merged Data Sets from Refs. 1 and 2:
# Ref.1: P.Dindinger report to Fat.Des.+Eval. Comm. Apr.2012
# Ref.2: G.A.Miller and H.S.Reemsnyder, "Strain-Cycle Fatigue of Sheet and
# Plate Steels I: Test Method Development and Data Presentation,"
# SAE Paper 830175, Detroit MI, Feb28-Mar.4, 1983
#
# NOTE that original test data ends at 2Nf = 1.3million.
#
#FileType= strain_life
#DataType= fitted
#TIMEcol= 0
#NAME= ASTM-A36
#NAME= Structural
#NAME= Steel
#Stress_units= ksi
#Strain_units= strain
#Sy= 38.4 0.2pc offset, 265 mpa
#Su= 69. ksi from Miller/Reemsnyder = 475 mpa
#eu= 0 #strain at Su not reported
#E= 29528. ksi = 203600 mpa
#FractureStrain= 0 not reported
#FractureStress= 0. not reported
#monotonic_K= 0 not reported
#monotonic_n= 0 not reported
#BHN= 138.
#%RA= 0. % not reported
#
#saedigcurve_v2.2.f starts.
# NOTE!! The Following Points are FITTED DATA:#NOTE!! Fitted Stress computed using E
# Total Strain 2Nf Stress Mean Plastic Strain Initial
# Amp Amp Stress Amp Elastic Mod.
0.88485 1 115.3 0. 0.88095 29528. #Fitted_point
0.00914 5000 52.1 0. 0.00737 29528. #Fitted_point
0.00665 10000 48.8 0. 0.00499 29528. #Fitted_point
0.00493 20000 45.7 0. 0.00338 29528. #Fitted_point
0.00344 50000 42.0 0. 0.00202 29528. #Fitted_point
0.00270 100000 39.3 0. 0.00136 29528. #Fitted_point
0.00217 200000 36.8 0. 0.00092 29528. #Fitted_point
0.00169 500000 33.8 0. 0.00055 29528. #Fitted_point
0.00144 1000000 31.6 0. 0.00037 29528. #Fitted_point
#Original test data ends at 2Nf = 1.3million.
#Points below are extrapolation:
0.00125 2000000 29.6 0. 0.00025 29528. #Fitted_point
0.00106 5000000 27.1 0. 0.00014 29528. #Fitted_point
#
#
```