## Using Crack Propagation Software

There are various commercially available programs, and probably a large number of individual programs, in existence for simulating crack propagation in engineering components. In this example we will be using an Open Source version which follows the recommendations of British Standard BS7910 closely.

A feature that has been added is the LIFO or Push-Down list material memory accounting system described in Chapter 5 of this tutorial. The Open Source type license that comes with the programs allows you to make software alterations to include any other features that you may wish to add. As usual there is of course **no warranty of any kind**. Please read the license at the top of the program listings and follow the web links to the full license terms.

The steps involved in computing damage or the propagation of a fatigue crack have been outlined in Chapter 8 of this tutorial. The present chapter section will demonstrate the use of the software to make predictions by means of an example.

The example simulates the tests and results by Kasra Ghahremani, "Predicting the Effectiveness of Post-Weld Treatments Applied under Load,", Link:

MSc. Thesis Civil Engr., U.Waterloo, Canada, 2010.

F.A.Conle Adjunct Prof U.Waterloo, 2017



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Details of the specimens and tests are available in the thesis and also at https://fde.uwaterloo.ca/Fde/CaseStudies/GhahremaniMSc/ghahremaniCase4.html

### **Material**:

CSA-350W (W=weldable) similar to ASTM-A572.:

G40.21-350W Simulated HAZ Constant Ampl. crack initiation Raw data

G40.21-350W Simulated HAZ Constant Ampl. crack initiation Fitted data

G40.21-350W Simulated HAZ Periodic Overstrain crack init. Raw data

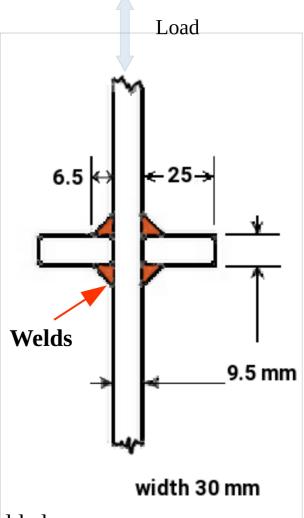
G40.21-350W Simulated HAZ Periodic Overstrain crack init. Fitted data

Crack Propagation da/dN data comparison plot

Crack Propagation da/dN Fitted data

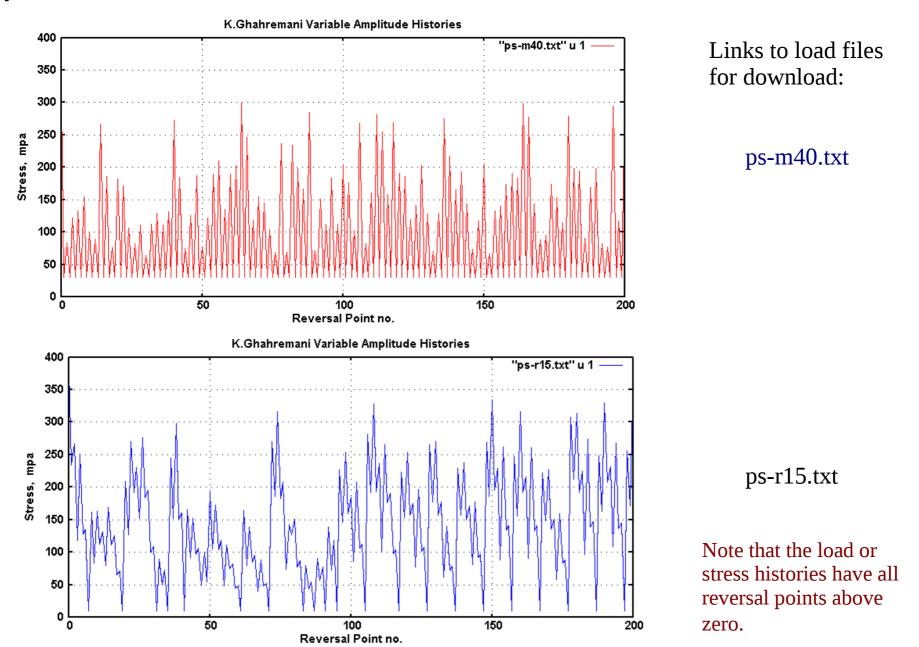
### **Geometry:**

The specimens are 30mm wide plates with full width lateral stiffeners welded to each side as shown in the figure. Specimens were cut in parallel from wider welded plates and then machined to 30mm widths. For good welds the expected stress concentration factor at the toe of weld is 1.8 to 2.0



### Loads:

The variable amplitude loading histories were observed on bridge members with loads generated by vehicles.



## Setup Software

1b. The folder CleanPdprop now consists of all the programs for crack propagation and also crack initiation; the latter using rainflow cycle counts as input. If you expect to be simulating several different problems it may save some time to leave the contents of CleanPdprop as-is and make a copy to some other folder e.g.:

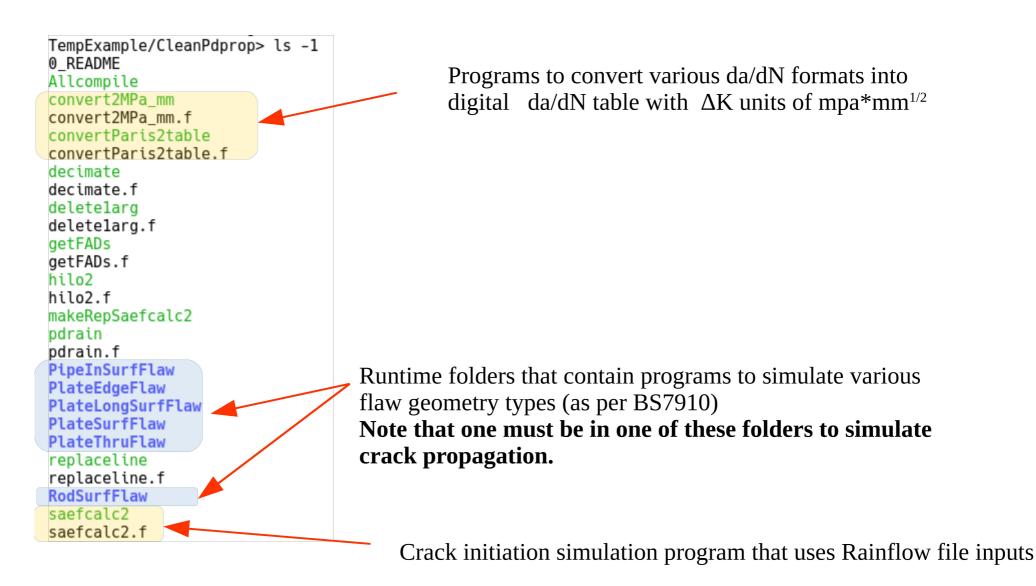
### cp -r CleanPdprop ~/Problem1/

This is a bit wasteful of disk memory, but it makes life easier when one has to return to a problem or simulation, after a period of time, to make changes.

1c. In order to make the pdf reports of simulation results you will also need to have available the programs: gnuplot and htmldoc

These are used by the makereport\* scripts.

## Files in CleanPdprop after Allcompile script is run



The non-highlighted files are programs that are also common to and used by the simulation programs in the blue highlighted folders.

Going into the Problem1/CleanPdprop/PlateSurfFlaw one sees the following files:

```
CleanPdprop/PlateSurfFlaw> ls
a36+1015.dadn
                                 makereport1
                                                               plateWeldflaw
a36+1015.dadn.user
                                 makereport1.bak
                                                               plateWeldflaw.f
a36_Mattos_mono_engrSS_FLAT.txt
                                                               plateWeldflaw range.f
                                 matfile
dadnTable
                                 merged_a36_fitted.html
                                                               plateWeldflaw+ss.f
examplOut.pdf
                                 merged_a36_fitted.html.user
                                                               plotFADs
fads.table
                                                               setup1
                                 mkfile00
α40.21-50A.dadn
                                 mkfile00 LoB=1.00
                                                               setup1.bak
g40.21-50A_non_os.fc.html
                                 mkfile90
                                                               SurfFlaw
g40.21-50A_non_os_fitted.html
                                 mkfile90_LoB=1.00
                                                               temp.loads
                                                               t_MmMb_Surflaw_00
q40.21-50A.paris
                                 pdprop.env
                                                               t MmMb Surflaw 90
load1.txt
                                 pdprop.env.bak
loadgp4
                                 pdprop.env.pwf
                                                               WeldSurfFlaw
loads4rain.out
                                 plateWeldFAD
makeInitReport
                                 plateWeldFAD.f
```

There are actually sufficient files, including example material files etc., to run the programs without adding any new user files, but we will go through the functions of the example files first before running the problems described in the previous pages of this chapter.

### Scripts:

```
is a script which checks the user files to see if all is present for a simulation.

setup1.bak is a backup copy of setup1 available in case someone clobbers setup1

makereport1 is a script which runs the simulation and presents the results in a *.html

report (also a *.pdf when htmldoc is available ) makereport1.bak is a backup.

It is a good idea to read over this script to understand what it is doing.

makeInitReport is a script to run only the crack initiation simulation. The script uses some

of the programs located in the folder ../CleanPdprop (above present folder)
```

TempExample/CleanPdprop> cd PlateSurfFlaw CleanPdprop/PlateSurfFlaw> ls -1 a36+1015.dadn Digital da/dN curves e.g.: a36+1015.dadn.user a36\_Mattos\_mono\_engrSS\_FLAT.txt cat a36+1015.dadn dadnTable examplOut.pdf #NAME = A36merged data from Newman, Haddad, Klingerman fads.table #Data digitized from merged graph in file a36+1015dadn-2.png g40.21-50A.dadn g40.21-50A\_non\_os.fc.html g40.21-50A\_non\_os\_fitted.html #deltaKunits= mpa mm g40.21-50A.paris #dadnunits= mm Units of data load1.txt in file loadgp4 # deltaK dadn loads4rain.out #MPa\*Sqrt(mm) dadn mm/cycle makeInitReport 150.216 9.62054e-08 makereport1 176.983 4.5623e-07 makereport1.bak 220.235 1.16017e-06 matfile 287.484 3.22409e-06 merged\_a36\_fitted.html 433.167 1.06976e-05 merged a36 fitted.html.user "fde-a36\_\_NewmanR0.1.tbl" u 1:2 "fde-a36\_\_NewmanR0.7.tbl" u 1:2 "haddadSAE1015dadn.tbl" u 1:2 #622.194 3.55031e-05 mkfile00 "klingermanR=0.11.tbl" u 1:2 "klingermanR=0.4.tbl" u 1:2 763.741 7.55681e-05 mkfile00 LoB=1.00 #950.39 0.000224548 0.01 mkfile90 1240.59 0.000852041 mkfile90 LoB=1.00 1471.68 0.0033073 pdprop.env 0.00 1675.69 0.0107468 pdprop.env.bak pdprop.env.pwf "#" character begins plateWeldFAD mm/cycle plateWeldFAD.f a comment line. plateWeldflaw (i.e.: not data) plateWeldflaw.f plateWeldflaw range.f plateWeldflaw+ss.f plotFADs setup1 **®** setup1.bak 000 œ SurfFlaw 1e-0 temp.loads t MmMb Surflaw 00 t MmMb Surflaw 90 WeldSurfFlaw 10000 Delta K, MPa\*sqrt(mm)

```
TempExample/CleanPdprop> cd PlateSurfFlaw
CleanPdprop/PlateSurfFlaw> ls -1
a36+1015.dadn
a36+1015.dadn.user
a36_Mattos_mono_engrSS_FLAT.txt
dadnTable
examplOut.pdf
fads.table
g40.21-50A.dadn
g40.21-50A_non_os.fc.html
g40.21-50A_non_os_fitted.html
q40.21-50A.paris
load1.txt
loadgp4
loads4rain.out
makeInitReport
makereport1
makereport1.bak
matfile
merged a36 fitted.html
merged_a36_fitted.html.user
mkfile00
mkfile00 LoB=1.00
mkfile90
mkfile90 LoB=1.00
pdprop.env
pdprop.env.bak
pdprop.env.pwf
plateWeldFAD
plateWeldFAD.f
plateWeldflaw
plateWeldflaw.f
plateWeldflaw range.f
plateWeldflaw+ss.f
plotFADs
setup1
setup1.bak
SurfFlaw
temp.loads
t_MmMb_Surflaw_00
t MmMb Surflaw 90
WeldSurfFlaw
```

## Tensile test Engr. Stress-Strain curve used to create FAD diagrams. (See BS7910 )

```
# A36 Steel Hot Rolled
# Machined from 5/8 inch hot rolled plate.
# Ref.: R.J.Mattos, F.V.Lawrence, "Estimation of the Fatigue Crack Initiation
# Life in Welds Using Low Cycle Fatigue Concepts," Fracture Control Rep.19
# Univ. of Illinois, Oct. 1975.
# NOTE!: For BS7910 FADs required Tags are:
    #FileType= #DataType= #Sy= #Su= #E=
    #Stress_units= #Strain_units=
#FileType= strain stress
#DataType= engineering
                         #Can be "engineering" or "true"
#NAME= ASTM-A36
#NAME= HotRolled
#NAME= Steel
#Stress units= mpa
#Strain units= strain
\#Sy = 224. mpa = 32.5 ksi
\#Su = 414. mpa = 60.0 ksi
#eu= 0.14 #strain at Su
#E= 190000 mpa 27500 ksi
#FractureStrain= 1.19
#FractureStress= 952 mpa = 138 ksi
#monotonic K= 780 mpa, 113 ksi
#monotonic n= 0.258
#BHN= 0. not reported
#%RA= 69.7 %
#From initial MattosStress-Strain plot
0 0
0.00036 72
0.00073 143
0.00146 224
0.00206 220
0.00274 224
...etc.
```

```
TempExample/CleanPdprop> cd PlateSurfFlaw
CleanPdprop/PlateSurfFlaw> ls -1
a36+1015.dadn
a36+1015.dadn.user
a36_Mattos_mono_engrSS_FLAT.txt
dadnTable
examplOut.pdf
fads.table
g40.21-50A.dadn
g40.21-50A_non_os.fc.html
g40.21-50A_non_os_fitted.html
g40.21-50A.paris
load1.txt
loadgp4
loads4rain.out
makeInitReport
makereport1
makereport1.bak
matfile
merged a36 fitted.html
merged_a36_fitted.html.user
mkfile00
mkfile00 LoB=1.00
mkfile90
mkfile90 LoB=1.00
pdprop.env
pdprop.env.bak
pdprop.env.pwf
plateWeldFAD
plateWeldFAD.f
plateWeldflaw
plateWeldflaw.f
plateWeldflaw range.f
plateWeldflaw+ss.f
plotFADs
setup1
setup1.bak
SurfFlaw
temp.loads
t_MmMb_Surflaw_00
t MmMb Surflaw 90
WeldSurfFlaw
```

Crack initiation axial fatigue tests data Fitted Curve files.

— used for crack initiation simulations. e.g.:

```
# NOTE: Fitted Data!!
# A36 Steel Merged Data Sets from Refs. 1 and 2:
# Ref.1: P.Dindinger report to Fat.Des.+Eval. Comm. Apr.2012
# Ref.2: G.A.Miller and H.S.Reemsnyder, "Strain-Cycle Fatigue of Sheet and
# Plate Steels I: Test Method Development and Data Presentation,"
# SAE Paper 830175, Detroit MI, Feb28-Mar.4, 1983
# NOTE that original test data ends at 2Nf = 1.3million.
#FileType= strain life
#DataType= fitted
#TIMEcol= 0
#NAME= ASTM-A36
#NAME= Structural
#NAME= Steel
#Stress units=ksi
#Strain units= strain
#Sy= 38.4 0.2pc offset, 265 mpa
#Su= 69. ksi from Miller/Reemsnyder = 475 mpa
        0 #strain at Su not reported
#eu=
#E= 29528. ksi = 203600 mpa
#FractureStrain= 0 not reported
#FractureStress= 0. not reported
#monotonic K= 0 not reported
#monotonic n= 0 not reported
#BHN= 138.
#%RA= 0. % not reported.
# NOTE!! The Following Points are <b>FITTED DATA:</b>
#NOTE!! Fitted Stress computed using Experm. K' and n'
#Total Strain 2Nf Stress Mean Plastic Strain Initial
# Amp
               Amp Stress
                             Amp
                                       Elastic Mod.
 0.88485
                        0. 0.88095
                                     29528. #Fitted point
              1 115.3
                         0. 0.00737 29528. #Fitted_point
 0.00914
            5000 52.1
                          0. 0.00499 29528. #Fitted point
 0.00665
            10000 48.8
            20000 45.7
                          0. 0.00338
                                       29528. #Fitted point
 0.00493
           50000 42.0
                          0. 0.00202
                                       29528. #Fitted_point
 0.00344
 0.00270
           100000 39.3
                          0. 0.00136
                                       29528. #Fitted_point
etc. . . . .
```

#### TempExample/CleanPdprop> cd PlateSurfFlaw CleanPdprop/PlateSurfFlaw> ls -1 a36+1015.dadn a36+1015.dadn.user a36\_Mattos\_mono\_engrSS\_FLAT.txt dadnTable examplOut.pdf fads.table q40.21-50A.dadn g40.21-50A\_non\_os.fc.html g40.21-50A\_non\_os\_fitted.html q40.21-50A.paris load1.txt loadgp4 loads4rain.out makeInitReport makereport1 makereport1.bak matfile merged\_a36\_fitted.html merged\_a36\_fitted.html.user mkfile00 mkfile00 LoB=1.00 mkfile90 mkfile90\_LoB=1.00 pdprop.env pdprop.env.bak pdprop.env.pwf plateWeldFAD plateWeldFAD.f plateWeldflaw plateWeldflaw.f plateWeldflaw\_range.f plateWeldflaw+ss.f time plotFADs setup1 Pm setup1.bak Pb SurfFlaw temp.loads t\_MmMb\_Surflaw 00 t MmMb Surflaw 90

WeldSurfFlaw

## **Load or stress history example: load1.txt**

```
# Test load history no. 1
# This history purposely has several material memory
# events which would mess up a simple range count method.
#time Pm Pb
    0 0
   7.5 30. #This point should be eliminated in peak pick
  17.5 70
  2.5 10
  15. 60
 -12.5 -50
  15 60
  2.5 10
  20. 80.
            #peak pick should eliminate
10 25. 100.
11 7.5
        30
             #peak pick should eliminate
12 3.75
        15.
13, 15,75
         63.
14. -12.5
         -50
15 15.75 63
   3.75
         15
17 17.5
         70
18
   5.0
         20 #peak pick should eliminate
```

In the histories there are three columns of data:

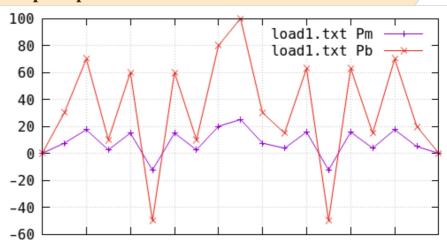
Membrane stress or load

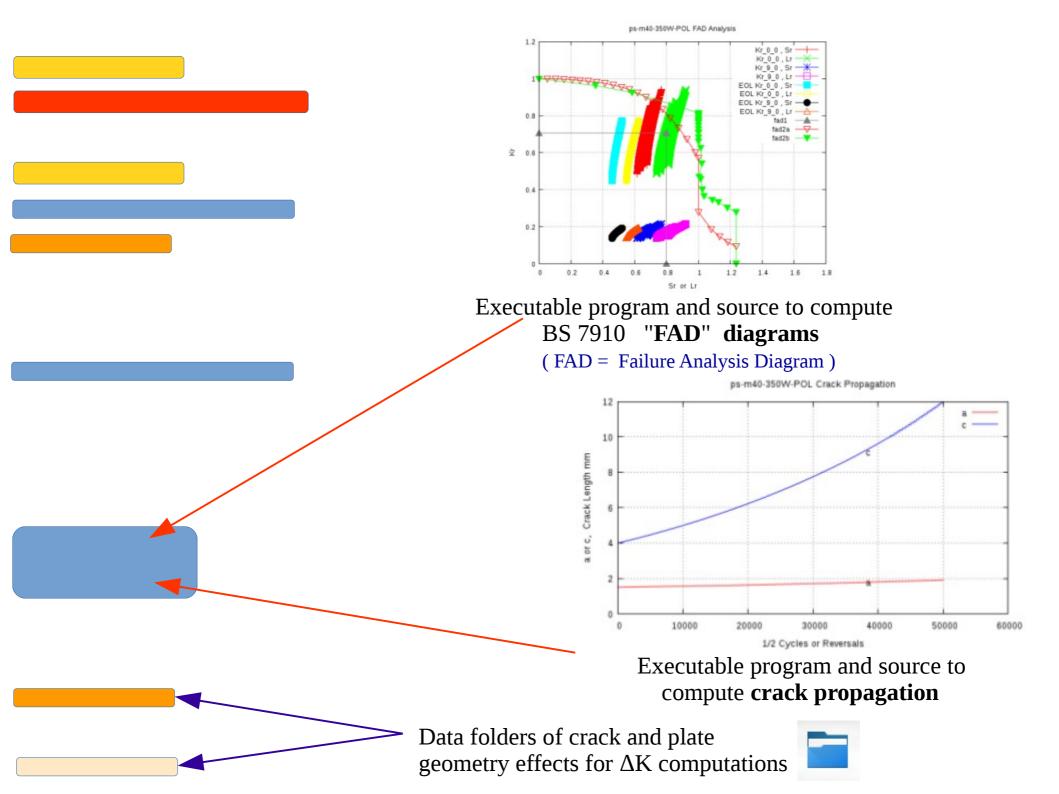
19

0 0

Bending stress or load

Pm and Pb are scaled up or down in control file pdprop.env





## **Run-time Control File: pdprop.env**

cat pdprop.env

```
# This file contains the starting filenames, variables etc
# for the Crack Propagation programs. It should be edited by the
# user before each simulation run.
#TYPE= plate_surface_flaw #with or without weld using ACTIVATEs:
#ACTIVATE_MmMb= 1
                             # Deactivate = 0
#ACTIVATE MkmMkb= 1
                             # Deactivate = 0 (0 implies NO weld )
#ACTIVATE_fw=
                  #Other
                            #TYPE= options:
                  # plate_long_surface_flaw
                  # plate tru flaw
                  # plate_embedded_flaw
                  # plate_edge_flaw
                  # pipe_inside_flaw
                  # pipe_full_inside_flaw
                  # pipe_full_outside_flaw
                  # rod_surface_flaw
                  # rod_full_outside_flaw
                  # These problem types are used to pull in the
                  # appropriate Fw, Mm, Mb, files etc.
# The factors described in this section may be ignored if not applicable to
# the particular problem type described above.
# (All dimensions in mm)
#B= 10.0 # plate (or pipe wall) thickness
#W= 70.0 # plate width
#ri= 200. # Internal diameter if pipe problem. Ignored if not pipe
#azero= 1.5 # initial crack depth
#czero= 4.0 # initial 1/2 crack width at surface
         # Weld Feature width. Ignored if ACTIVATE_MkmMkb= 0 (above)
\#L = 10.
```

### continued on next page

### **Run-time Control File:** pdprop.env (page 2)

```
#HISTORYFILE= load1.txt # historyFileName
       # Adjustments to load file variables:
#
       # Note that the MEANADD (below) is added AFTER the MAGFACTOR is applied.
#MAGFACTOR_m= 1.0 # Multiply factor on membrane load. Result should be MPa
#MAGFACTOR_b= 1.0 # Multiply factor on bending load term. Result should be MPa
#MEANADD m= 0.0 # Mean shift in MPa added to membrane stress.
#MEANADD b= 0.0 # Mean shift in MPa added to bending stress.
#MAXREPS= 1000000 # Max no. history repeats in simulation.
             # One repetition or application of the load history is
             # also called a "block" of cycles.
#
#MATERIAL= merged_a36_fitted.html #File name of material fitted data
                   This file is used to define the cyclic
#
#
                   stress-strain curve, and the Neuber Product curve.
               #Stress Conc. Factor, presently only for crack initiation calcs.
\#Kt= 2.0
#
#DADN= table
                            # Can be "table" or "Paris"
#DADN PARIS= 0.0 0.0 0.0 none # Kth a m Kc units (ignored if #DADN= table)
#DADN_TABLE= a36+1015.dadn # da/dN digitized da/dN curve for material,
                   including the threshold, and KIc.
#
                   If a threshold exists, put in a vertical line
#
#
                   (with two identical X-axis points).
                   If the threshold needs to be "turned off" then
#
#
                   do NOT put in a vertical line at low da/dN.
#
                   (Ignored when #DADN= PARIS)
```

## **Run-time Control File:** pdprop.env (page 3)

```
#FAD Stuff:
#TensileFile= a36_Mattos_mono_engrSS_FLAT.txt #enter "none" if no FAD
                     #Set these so that Pm+Pb= 0.82*Syield for default.
#PmEOL= 70.
#PbEOL= 100.
                           "EOL" stands for "End of Life"
\#Kmat= 1675.
#PinJoint= 0
                     #Set = 1 if structure is pin-Jointed (for bending)
#
#BLOCKSKIP= 1.0 percent # At the end of each block check if the previous
#
                    two blocks of cycles had similar damage (crack
                    extension) within this percentage. If TRUE then
                    simply skip the simulation of the next block,
#
                    but just add the expected damage. Continue by
#
#
                    simulating the block after the skip.
#
                    A value of 0.0 will disallow skipping blocks.
                    (this feature is not ready yet. 0.0 is assumed)
#
#SAVELEVEL= 0
                          #Amount of output saved to disk:
                 # 3=lots 2=medium 1=minimal
#
#
                 # 0= save #crk= data into binary direct access file only
#
                      No #crk= data will be written into the text logfile.
#
                      Use for large output files with lots of cycles.
                  (End of pdprop.env control file)
```

Note that there are a number of other files in the folder PlateSurfaceFlaw but they are not relevant for this example.

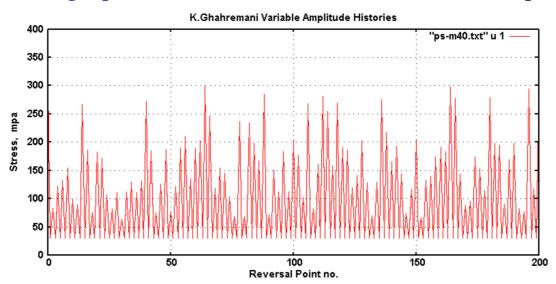
Background information: K.Ghahremani MSc. Thesis Civil Engr., U.Waterloo, Canada, 2010.

Step 1: As described in the previous pages of this chapter, we have downloaded a copy of the crack propagation programs, compiled them, and are now in a folder such as ..../CleanPdprop/PlateSurfFlaw

Step 2a: If you have not already done so, download Ghahremani's load file ps-m40.txt Use vi or gvim to take a look at the contents. Generally it is a good idea to check at least the top and bottom of such a file. The format for each data line in the file is

Point-No. Pm Pb No.Reps.

Only Pm (Membrane stress) and Pb (Bending stress) are used by the program at this time. Note that, in this case, all the Pb values are 0 i.e.: no bending You can also use gnuplot to check if the values are similar to the plot below.



Or try: hilo2 <ps-m40.txt to check max and mins.

Step 2b. Enter the name of the file ps-m40.txt into the pdprop.env control file

Step 2c. Use the magnification and mean shift factors to scale the Pm and Pb values. In this case the values in ps-m40.txt do not need any scaling or shifting.

```
# (All dimensions in mm)

#B= 10.0 # plate (or pipe wall) thickness

#W= 70.0 # plate width

#ri= 200. # Internal diameter if pipe problem. Igno

#azero= 1.5 # initial crack depth

#czero= 4.0 # initial 1/2 crack width at surface

#L= 10. # Weld Feature width. Ignored if ACTIV

#HISTORYFILE= ps-m40.txt # historyFileName

# # Adjustments to load file variables:

# # Note that the MEANADD (below) is added....

#MAGFACTOR_m= 1.0 # Multiply factor on memb

#MAGFACTOR_b= 1.0 # Multiply factor on bendi

#MEANADD_m= 0.0 # Mean shift in MPa added ...

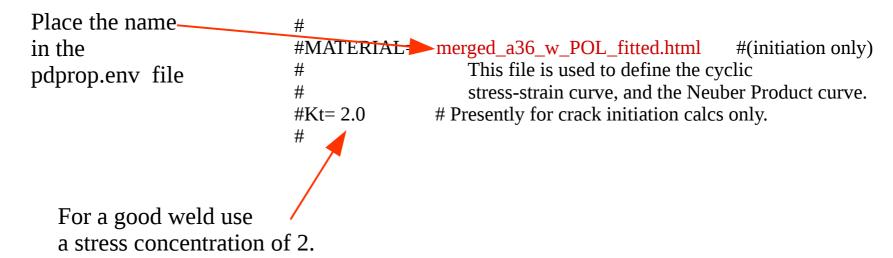
#MEANADD_b= 0.0 # Mean shift in MPa added ...
```

## Step 3. Provide a file for **crack initiation** calculations.

Ghahremani in his MSc thesis did not provide crack initiation test data, so we will use an approximation; specifically a data set for A36 steel which has similar carbon content but lower yield stress. It is a periodic overload (POL) data set.

### Fitted initiation file for dowload:

https://fde.uwaterloo.ca/FatigueClass/Chap10Using/merged\_a36\_w\_POL\_fitted.html.txt (Note: remove the ".txt" suffix using rename or mv )

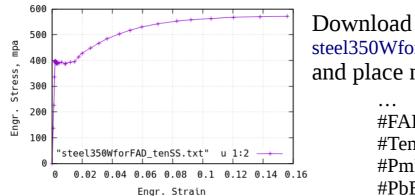


Step 4.: Specify crack propagation curve: da/dn vs ΔK information Generally it is easiest to provide about 10 digitized points that are on your best estimate of the da/dn curve to use. Straight line interpolations between the points are made during the simulations.

# # Enter: "table" or "Paris" #DADN= table If you are using a file #DADN\_PARIS= 0.0 0.0 0.0 0.0 none #(ignored if #DADN= table ) of digital points place m Kc units Kth the word "table" here. !! For units specify: mpa\_m or ksi\_in or mpa\_mm ksi in: ksi stress, inch crack length, inches in delta K mpa m: mpa stress, m crack length, meters in delta\_K # mpa\_mm: mpa stress, mm crack length, mm in delta\_K # same as  $N/(mm^{**}(3/2))$ #DADN\_TABLE= g40.21-350W.dadn # da/dN digitized da/dN curve, (ignored when #DADN= PARIS ) includes digital threshold, and KIc. In this example we will If a threshold exists, put in a vertical line use Ghahremani's da/dn (with two identical X-axis points). curve of which there is If the threshold needs to be "turned off" then a digital text file available. do NOT put in a vertical line at low da/dN. Download: g40.21-350W.dadn.txt remove the ".txt" suffix from the filename.

Then enter the filename here.

Step 5: Provide a tensile test stress-strain curve for the FAD (Failure Assessment Diagram) if available. BS 7910: "The vertical axis of a FAD is a ratio of the applied conditions, in fracture mechanics terms, to the conditions required to cause fracture, measured in the same terms. The horizontal axis is the ratio of the applied load to that required to cause plastic collapse."



BS 7910: "If a valid  $K_{\rm IC}$  is available Kmat should be taken as  $K_{\rm IC}$  "

steel350WforFAD\_tenSS.txt
and place name here
...

#FAD Stuff:

#TensileFile= steel350WforFAD\_tenSS.txt #enter none if no FAD

#PmEOL= 200. #Set these so that Pm+Pb= 0.82\*Syield for default.

#PbEOL= 90. ("EOL" implies End Of Life)

#Kmat= 4300.

#PinJoint= 0 #Set = 1 if structure is pin-Jointed (for bending)

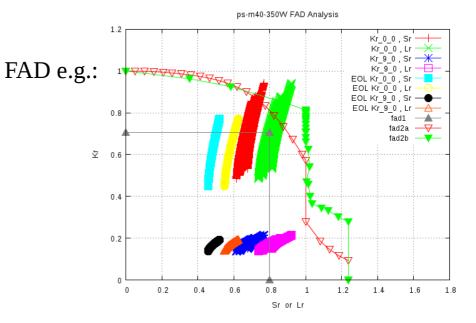
#

If no file is available

enter none here.

For further explanation of the FAD please refer to BS 7910:2005 Section 7:

"Assessment for fracture resistance"



Step 6: Define the specimen/problem type and activate the necessary finite width etc. modification factors.

**Mm** and **Mb** are stress intensity magnification factors for membrane and bending.

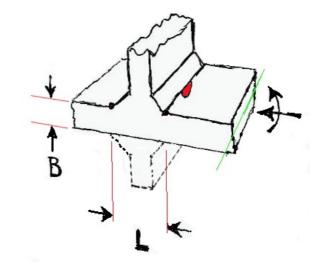
**Mkm** and **Mkb** are stress intensity magnification factors in the presence of stress raisers; in this case due to the weld.

**fw** is a finite width correction factor for elliptical flaws.

```
#TYPE= plate_surface_flaw #with or without weld using ACTIVATEs:
#ACTIVATE MmMb= 1 # Deactivate = 0
#ACTIVATE MkmMkb= 1
#ACTIVATE fw=
                  #Other
                           #TYPE= options:
#
                  # plate_long_surface_flaw
#
                  # plate_tru_flaw
                  # plate embedded flaw
                  # plate edge flaw
                  # pipe inside flaw
                  # pipe_full_inside_flaw
                  # pipe_full_outside_flaw
                  # rod surface flaw
                  # rod full outside flaw
                  # These problem types are used to pull in the
#
                  # appropriate Fw, Mm, Mb, files etc.
#
```

Step 7: Define the specimen dimensions, the initial crack size, and the weld feature size L.

,,,



#The factors described in this section may be ignored if not applicable to # the particular problem type described above.

# (All dimensions in mm)

#B= 9.5 # plate (or pipe wall) thickness

#W= 30.0 # plate width

#ri= 00. # Internal diameter if pipe problem. Ignored if not pipe

#azero= 1.5 # initial crack depth

#czero= 4.0 # initial 1/2 crack width at surface

#L= 22.3 # Weld Feature width. Ignored if ACTIVATE\_MkmMkb= 0 (above)

Step 8: Run the setup check script. In this case: setup1 ./setup1

It will check some of your files and parameters in pdprop.env for correct format. The script asks the user questions and allow the user to make changes if required. It also creates the tables for Mm, Mb etc for your given geometry and problem type. At the end of this script you will get some text as to how to run the simulation. It would be a good idea to read over the script now.

Step 9: Run the simulation. The general format of this command is : ./plateWeldflaw scaleFactor <loadHistory >outputFile

By changing the scaleFactor you can increase or decrease the stresses in the load history. e.g.:

./plateWeldflaw 0.95 <load1.txt >plateXYZout0.95

./plateWeldflaw 0.90 <load1.txt >plateXYZout0.90

In our case we can run the simulation, after the previous steps with the command: ./plateWeldflaw 1.0 <ps-m40.txt >ps-m40-350W-POL

If you expect lots(millions) of cycles check the size of the output file as the simulation is running with the command:

ls -lt | head -12

or

**in another terminal window**. The output file contains information about every half cycle and this file may get bigger than what you would like.

Step 10: After the simulation has ended you can generate a report using the makereport script. ./makereport1 outputfile

In our example case:
./makereport1 ps-m40-350W-POL

The makereport scripts read the random access output file and create a number of plots and text information. The plots will appear as files in your present folder, as will an HTML file that gathers the plots into a report format. If the system program "htmldoc" is present the script will also create a pdf file of the report.

e.g. pdf report:

ps-m40-350W-POL.pdf