

# Small Specimen Testing for Basic Fatigue Properties

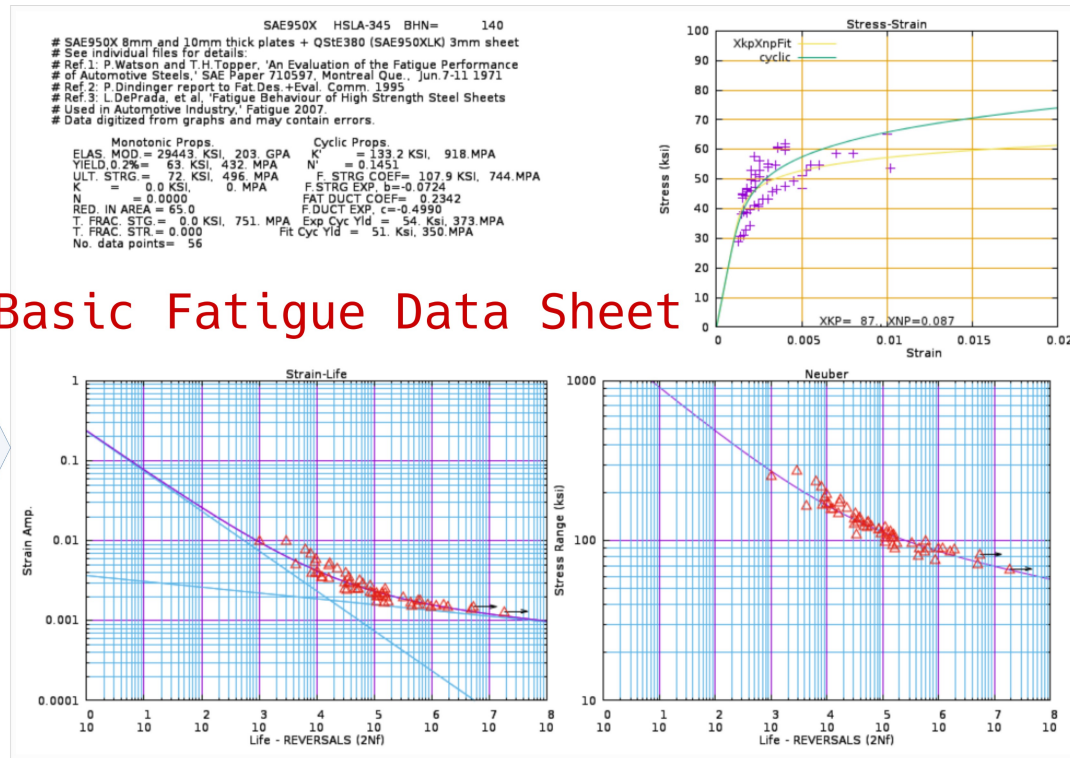
Philosophy:

Test small specimens for basic fatigue data.  
Then design components & structures.

Axial  
loaded  
specimen



## Basic Fatigue Data Sheet



Component

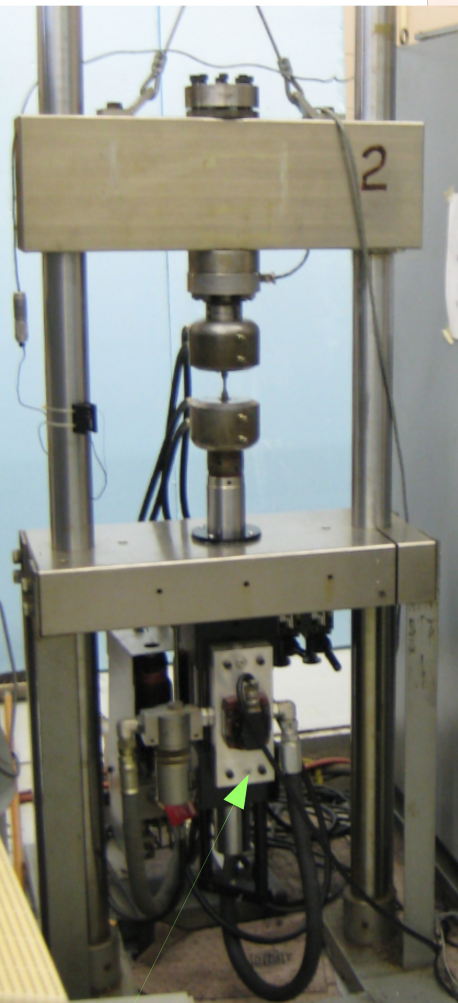


Objective

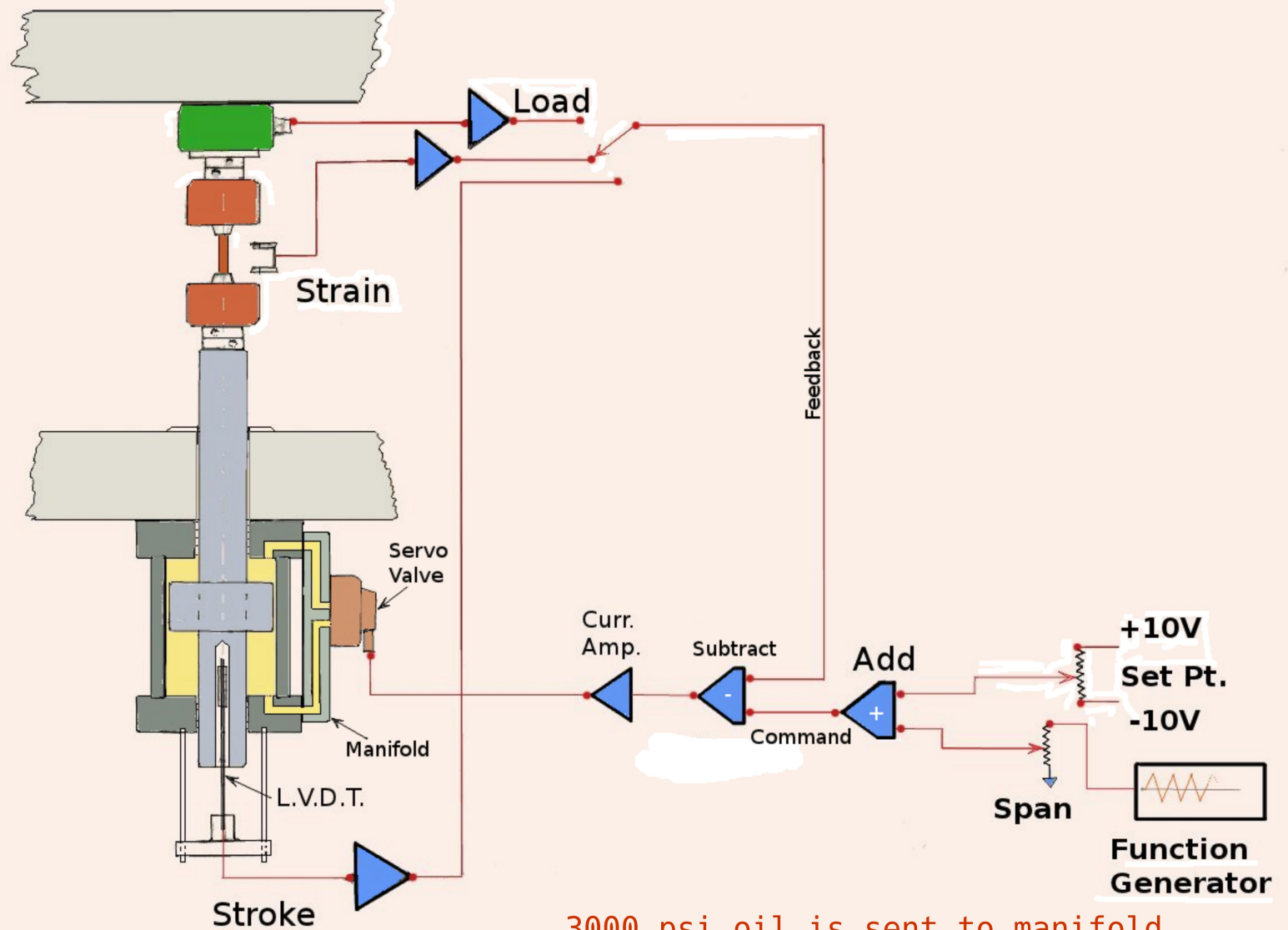
With good design: Only 1 final component test is needed

Servo-hydraulic test machines are used for small specimen testing.

If you are going to be involved in tests, make sure you understand this schematic.



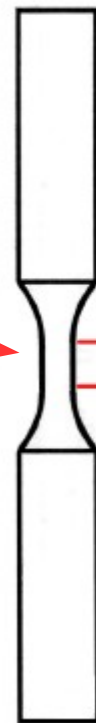
Manifold



3000 psi oil is sent to manifold from remote hydraulic pump



Load Cell



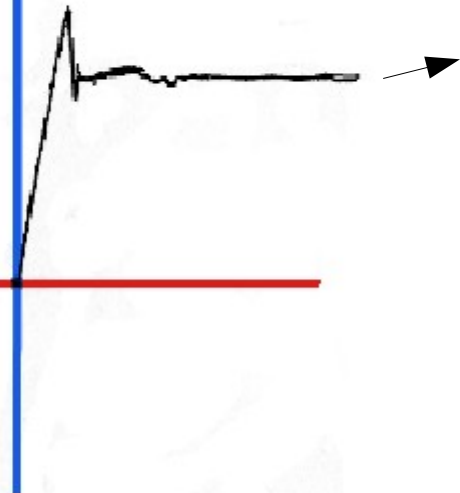
Extensometer



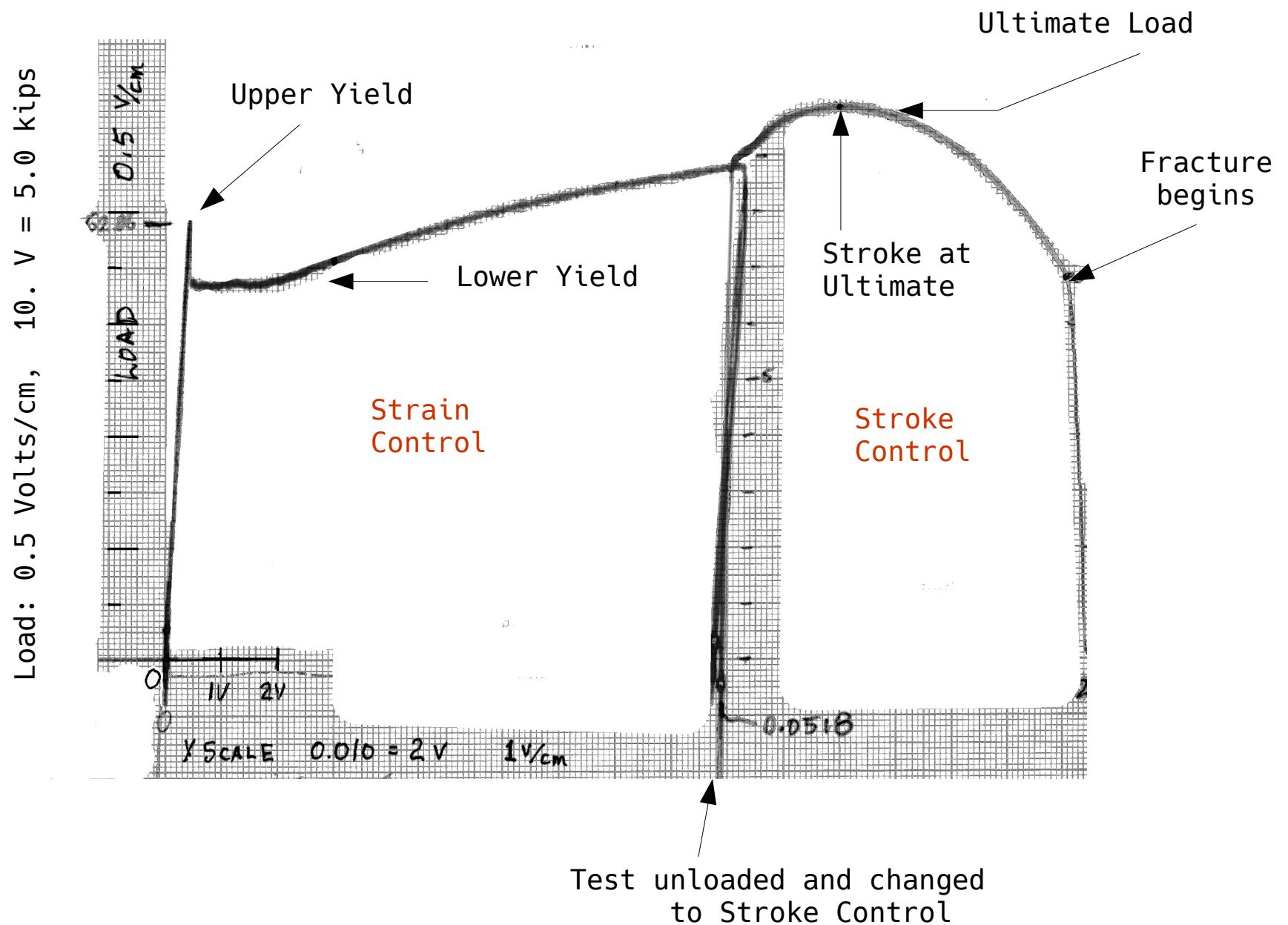
X

Y

0

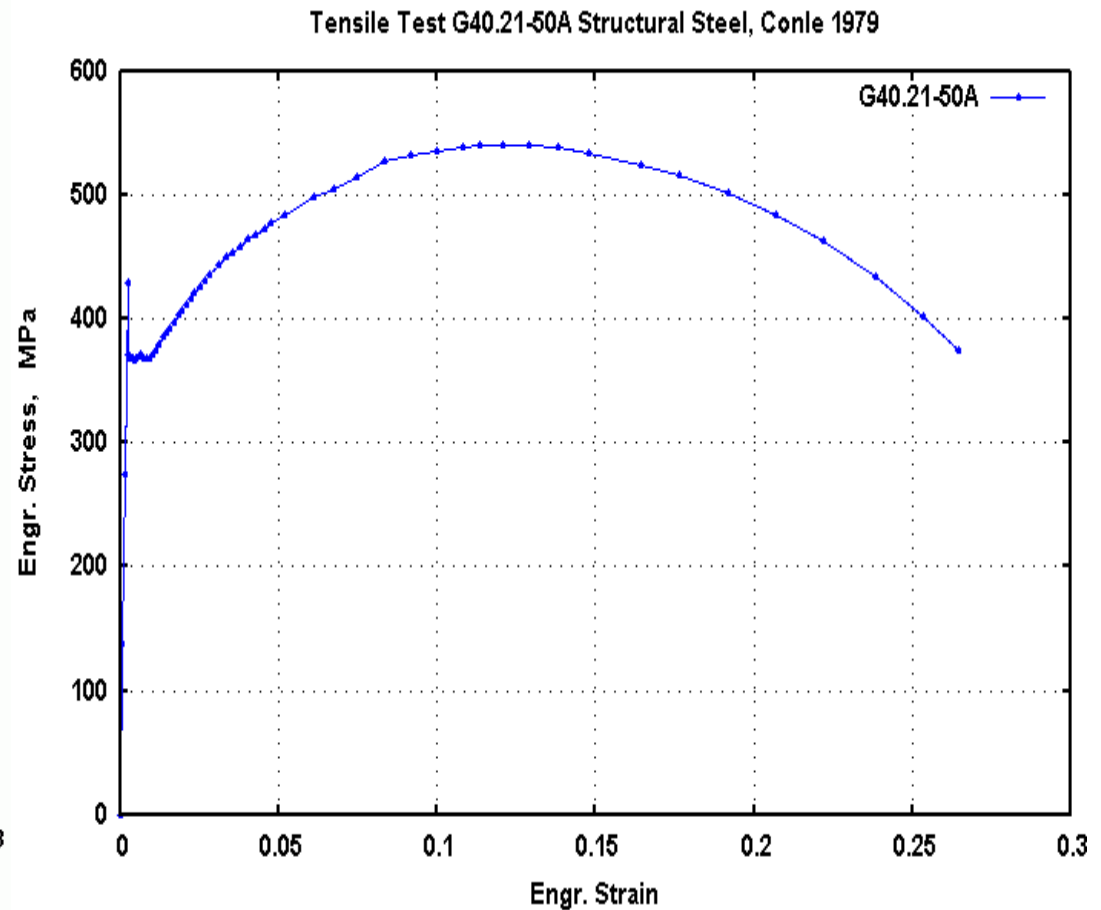
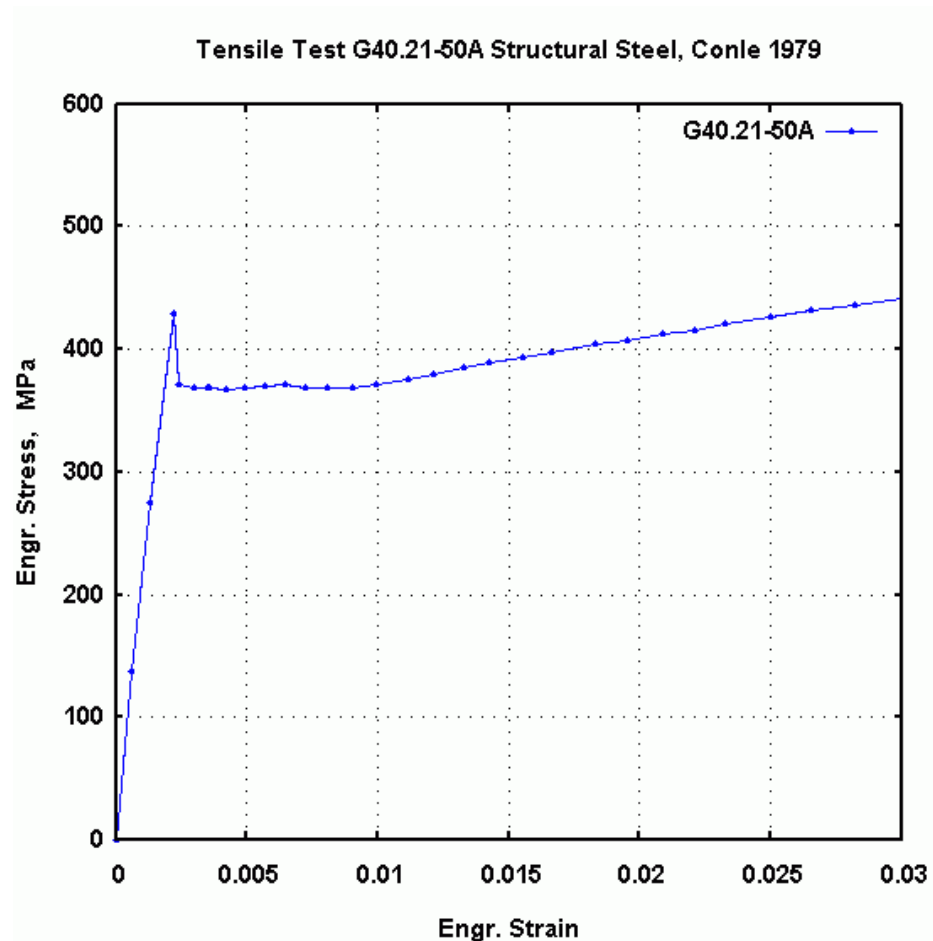


Typical Tensile Test: Raw data on X-Y Plotter Paper;  
(most of grid paper removed)



After completion the test data can be digitized, or already may be in computer form. Using gnuplot one can create a gif animation of the test:

<https://fde.uwaterloo.ca/FatigueClass/Videos/g40-21TensileData.gif> ( 1.2 Mb )



Example of digitized data:

<https://fde.uwaterloo.ca/Fde/Materials/Steel/Other/Astm-A588C/astm-A588C.html>



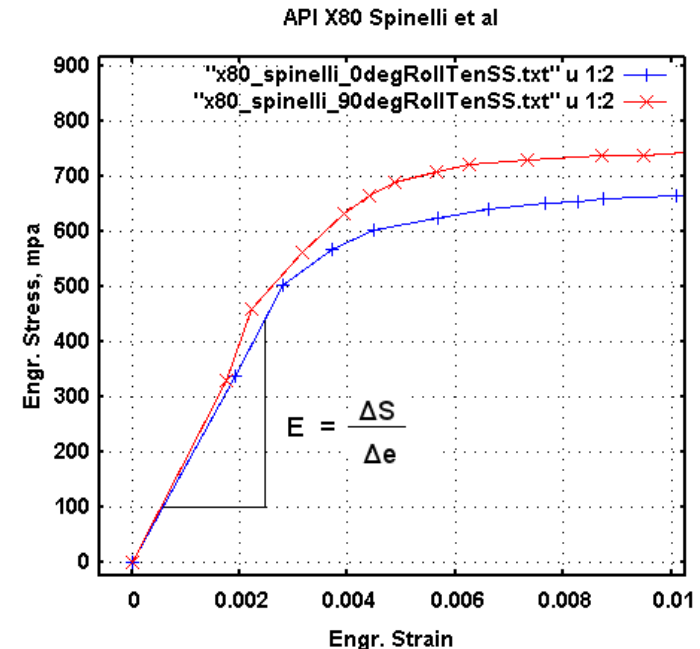
For fatigue design applications Tensile Test parameters serve primarily as material characterization values, much like a hardness test number.

The values are used as a check to answer: “Do I have the right material?”

Values you should request from a supplier or tester:

|                          |                |                |
|--------------------------|----------------|----------------|
| Elastic Modulus          | E              | (stress units) |
| 0.2% Offset yield Stress | S <sub>y</sub> | “              |
| Ultimate Tens. Stress    | S <sub>u</sub> | “              |
| True Fracture Stress     | σ <sub>f</sub> | “              |
| Strain at Ultimate       | e <sub>u</sub> | (strain units) |
| True Fracture Strain     | ε <sub>f</sub> | “              |

Hardness



If you are working with a component you should consider cutting a tensile sample from it and test it to check your assumptions. At the very least check the hardness.

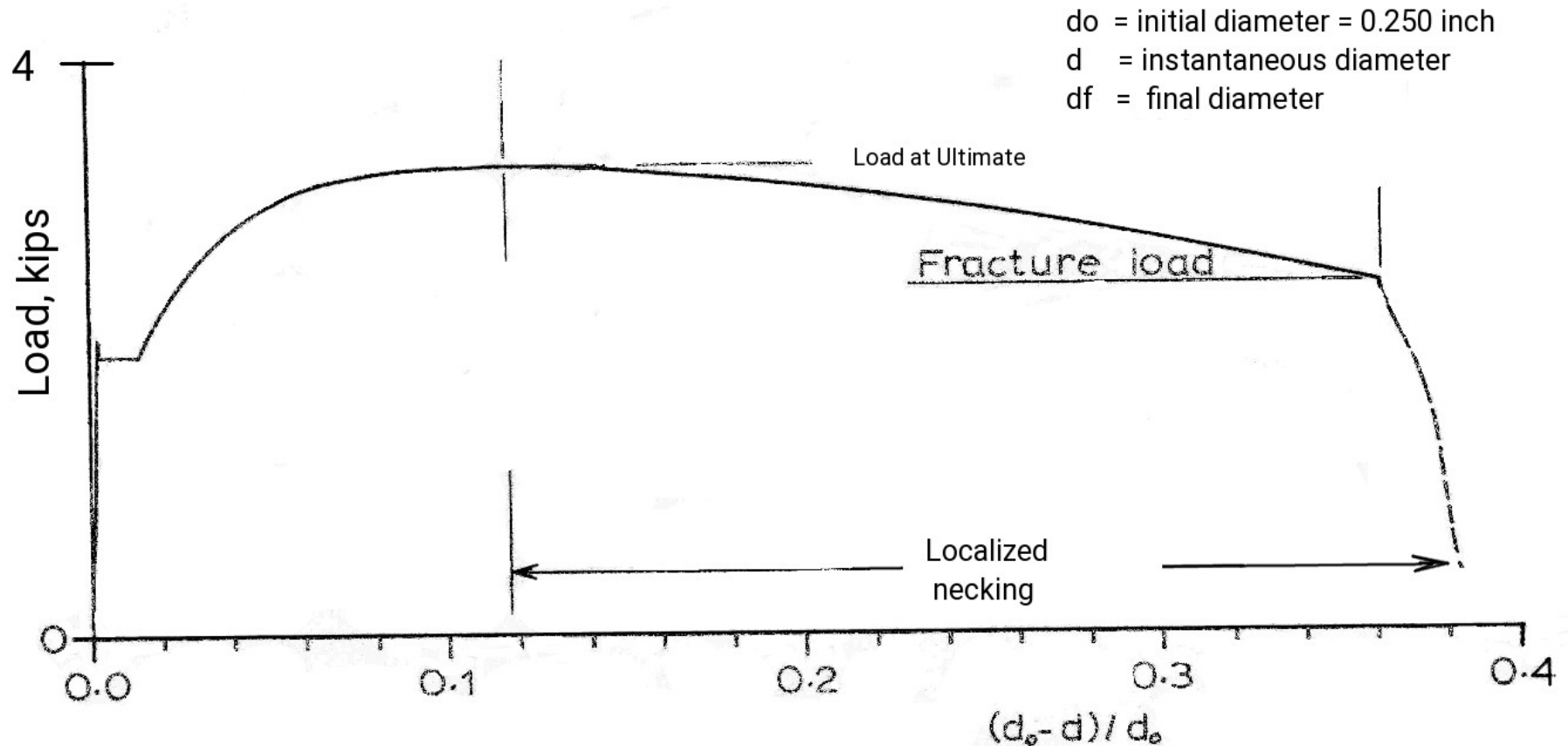
Note that fatigue cycling can change some of these values, so use a new component/specimen.

# Exercise

Digitize and plot the tensile curve in picture below

1. Use a digitizer such as “engauge”  
<https://github.com/markumitchell/engauge-digitizer/releases>
2. Plot your digital results using “gnuplot”  
<https://sourceforge.net/projects/gnuplot/files/gnuplot/>

Diametral tensile test of Normalized SAE1015



See also next page

Notes for exercise on previous page;

- (a) In order to use the **engage** digitizer one needs to have an image of the curve(s). Thus for this exercise you will need to take a **screenshot** of the tensile curve on previous page.
- (b) In engage use the **import** option to load your image
- (c) Select a **Zoom** level to make it easy to click on important points
- (d) Check your **Settings → Co-ordinates** to ensure you have linear (in this case)
- (e) Click on **Axis Point Tool** to set the three plane definition points
- (f) Click on **Curve Point Tool** to pick the points on the curve
- (g) When done **File → Export** the points to a \*.csv file.  
Use **SPACE delimited** data for gnuplot

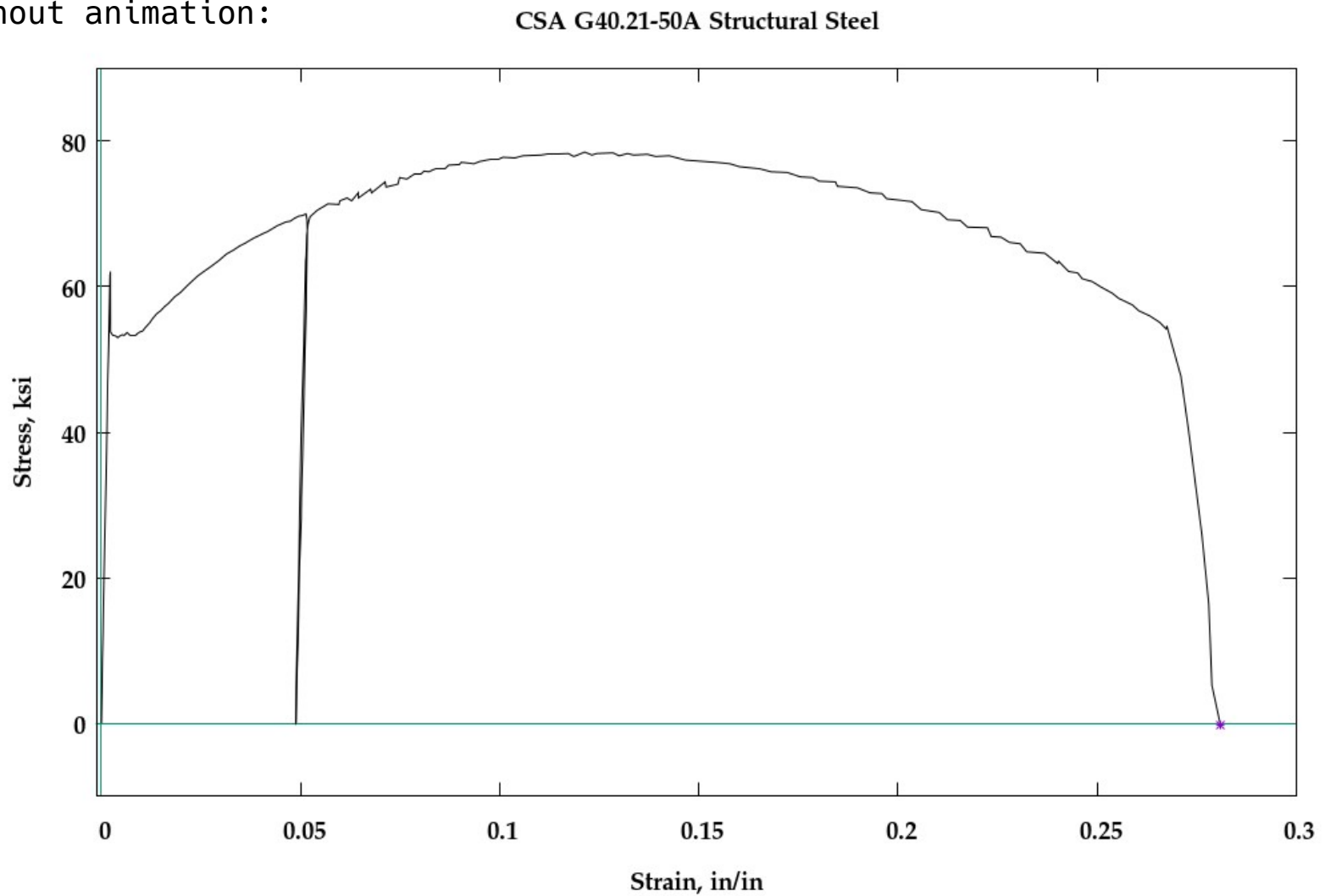
- (a) In **gnuplot** make sure you are in the correct folder which contains your data
- (b) If you have saved the digitized data (space delimited) to **example.csv** you can use the following commands to create plots:  
gnuplot> **set term x11 enhanced font "arial,20"**  
gnuplot> **set grid**  
gnuplot> **plot "example.csv" using 1:2 with linespoints**  
or  
gnuplot> **plot "example.csv" u 1:2 w lp**  
gnuplot> **set ylabel "Stress, ksi"**  
gnuplot> **plot "example.csv" u 1:(\$2/0.049) w lp**
- (c) You can **zoom** using the **right mouse button**. Then type **"p"** to go back.
- (d) In lower left corner of window you will see the mouse co-ordinates in plot



In stress vs. strain co-ordinates the resulting digitization can be displayed in an animation. e.g.:

<https://fde.uwaterloo.ca/FatigueClass/Videos/g40-21TensileData.gif> (1.Mb)

Plot without animation:



# Un-notched Axial Specimen testing for basic fatigue properties

Objective: Create data for SAE standard fatigue file and make data plots

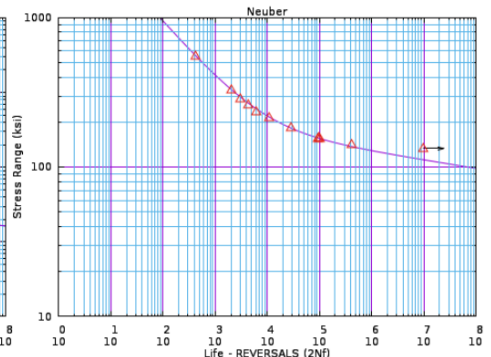
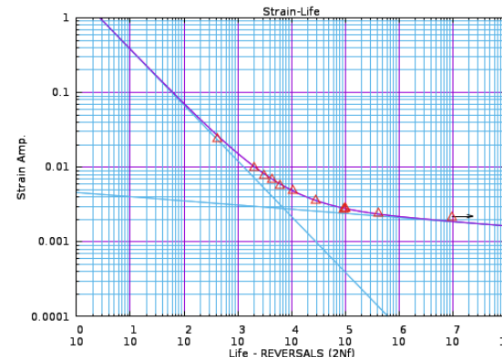
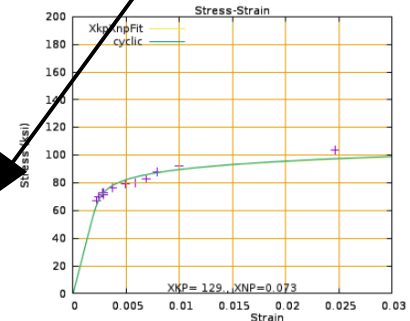
From:

<https://fde.uwaterloo.ca/Fde/Materials/Steel/BoronSteel/boronSteel.html>

```
#FileType= strain_life
#DataType= raw
#TIMEcol= 0
#NAME= UoWaterloo
#NAME= SAE10B20_Steel
#Stress_units= ksi
#Strain_units= strain
#Su= 121.00
#Sy= 110.00
#E= 30000.
#%RA= 0.0 Not reported
#BHN= 231.
```

```
#NO. FAT. PTS.= 12
#Tot Strain 2Nf Stress Mean Plas.Strain Initial
## Amp Amp Sts Amp ElasticMod.
0.024650 425. 104.00 0. 0.021180 30000.
0.010000 2031. 92.00 0. 0.006930 30000.
0.007950 3076. 88.00 0. 0.005020 30000.
0.006900 4283. 83.00 0. 0.004130 30000.
0.005830 6201. 80.00 0. 0.003160 30000.
0.004920 10611. 79.00 0. 0.002290 30000.
0.003710 28893. 76.50 0. 0.001160 30000.
0.002900 98546. 73.00 0. 0.000467 30000.
0.002850 100012. 71.50 0. 0.000467 30000.
0.002780 92800. 73.00 0. 0.000347 30000.
0.002440 417400. 70.00 0. 0.000107 30000.
0.002210 9661220. 67.00 0. 0.000000 30000.
```

```
UoWaterloo SAE10B20g BHN= 231
# SAE10B22 quenched + temp to Rc=35. The 1/2in
# plate was retempered at 1620F for 3hrs to avg. core hardness
# of Rc=21. Material supplied by Caterpillar Tractor Co.
# Cylindrical spec., 0.3in GL, parallel to roll dir..
# ground + polished after machining
# SAE10B20 chemistry 0.20C 1.32Mn .009P .010S .27Si .01Ni
# 02Cr .01Cu .05Al .050Ti 0.00096Boron
# Sample with 425 life is a diametral test.
# Ref: F.A. Conle, 'A Computer Simulation Assisted Statistical
# Approach to the Problem of Random Fatigue,' MSc Thesis
# Univ. of Waterloo, March 1974.
# Amp Stress Amp Elastic Mod.
Monotonic Props. Cyclic Props.
ELAS. MOD.= 30000 KSI, 207 GPa K' = 130.1 KSI, 897 MPA
YIELD. 0.2% = 110 KSI, 758 MPA N' = 0.0751
ULT. STRG = 121 KSI, 834 MPA F. STRG COEF = 137.6 KSI, 948 MPA
K = 0.0 KSI, 0 MPA F. STRG EXP. b = -0.0559
N = 0.0000 FAT DUCT COEF = 2.0907
RED. IN AREA = 0.0 F DUCT EXP. c = -0.7450
T. FRAC. STG = 0.0 KSI, 0 MPA Exp Cyc Yld = 82 KSI, 563 MPA
T. FRAC. STR = 0.000 Fit Cyc Yld = 82 KSI, 563 MPA
No. data points = 12
```



#Diametral

#Runout

Then check data and make "Fitted Curve" file for fatigue design.

Ok, lets simulate the fatigue test process.

Actions:

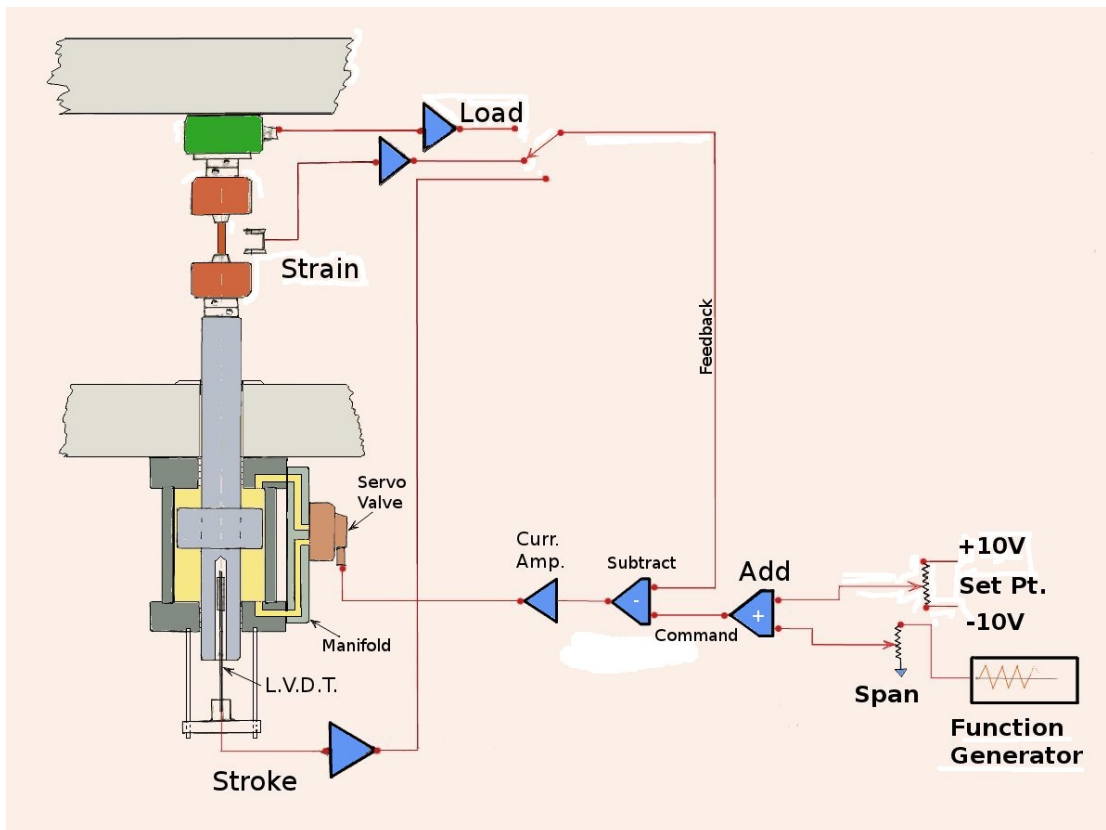
Set servo-hydraulics into Load feedback  
(also called Load Control )

Place the axial unnotched specimen into the grips.

Mount the calibrated extensometer on the specimen.

Set load to zero, strain to zero

Switch to Strain feedback ( Strain Control )



Lets “test” a fatigue specimen. Place machine in Strain feedback control.  
Set the program triangular waveform to achieve max strains of 0.01 in Tension and -0.01 in compression. Place “Set Point” at 0.0 strain.  
Start the computer or function generator waveform.

Animation:

[https://fde.uwaterloo.ca/FatigueClass/Videos/bSteel\\_tStart.gif](https://fde.uwaterloo.ca/FatigueClass/Videos/bSteel_tStart.gif)(3.3Mb)

The max or mins at which the stress and strain change direction are called **Reversal** points

The curve between two reversals is called a **Half-Cycle**

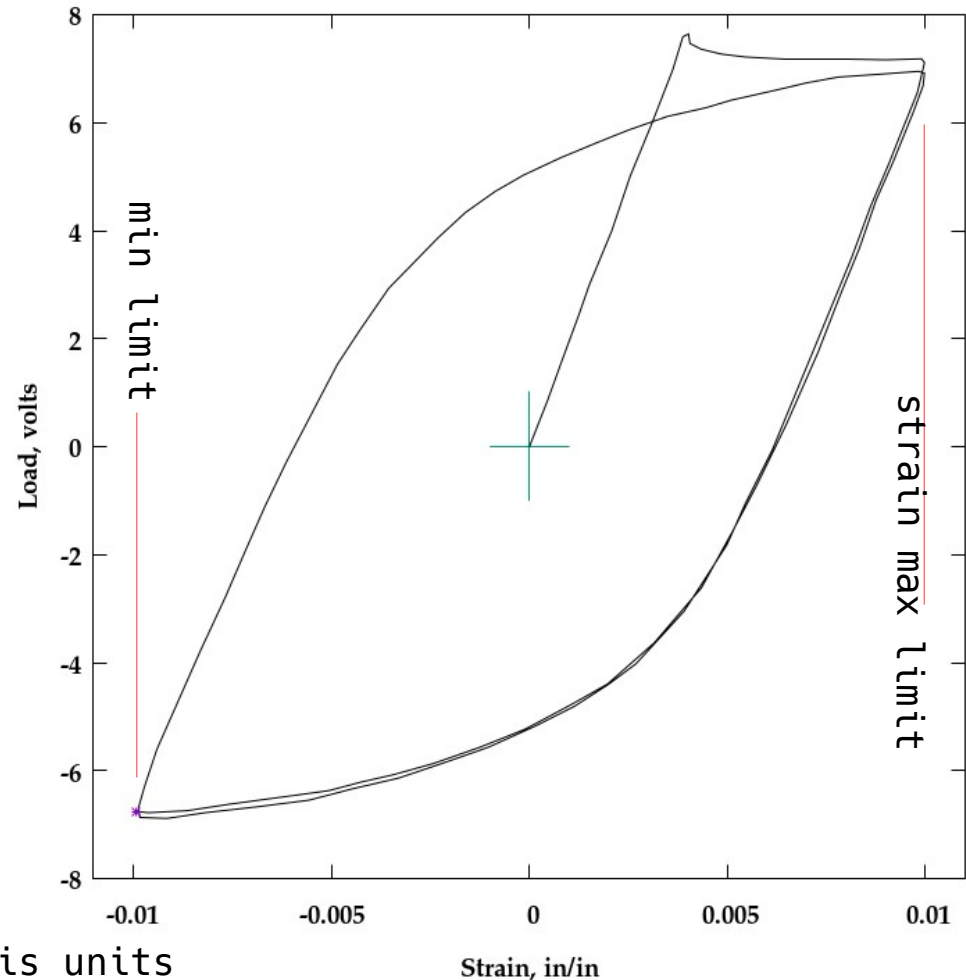
and in the same vein two half-cycles constitute a **Cycle**.

The stress-strain shape defined by a cycle is called a **Hysteresis Loop**.

People generally count the number of cycles or reversals to define Fatigue life.

$N_f$  = Cycles to failure

$2N_f$  = Reversals to failure



Y axis units  
have been left  
in volts

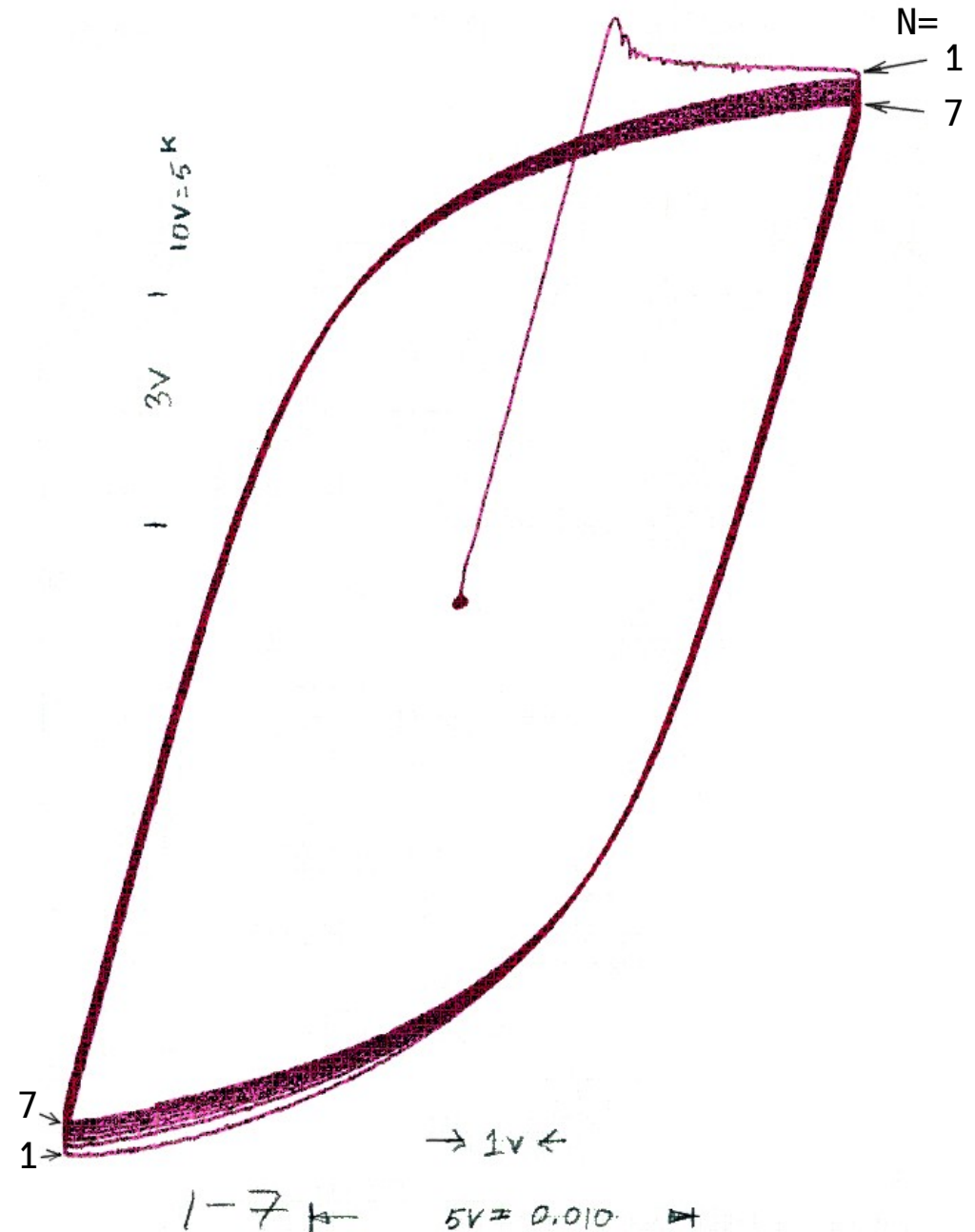
Here is the same plot as taken directly from the graph paper. The graph grid has been removed. Only the first 7 cycles of the test are shown.

This test, if run to failure, would fracture in about  
1000 cycles

Also notice that the load peaks are changing slightly with each half cycle.

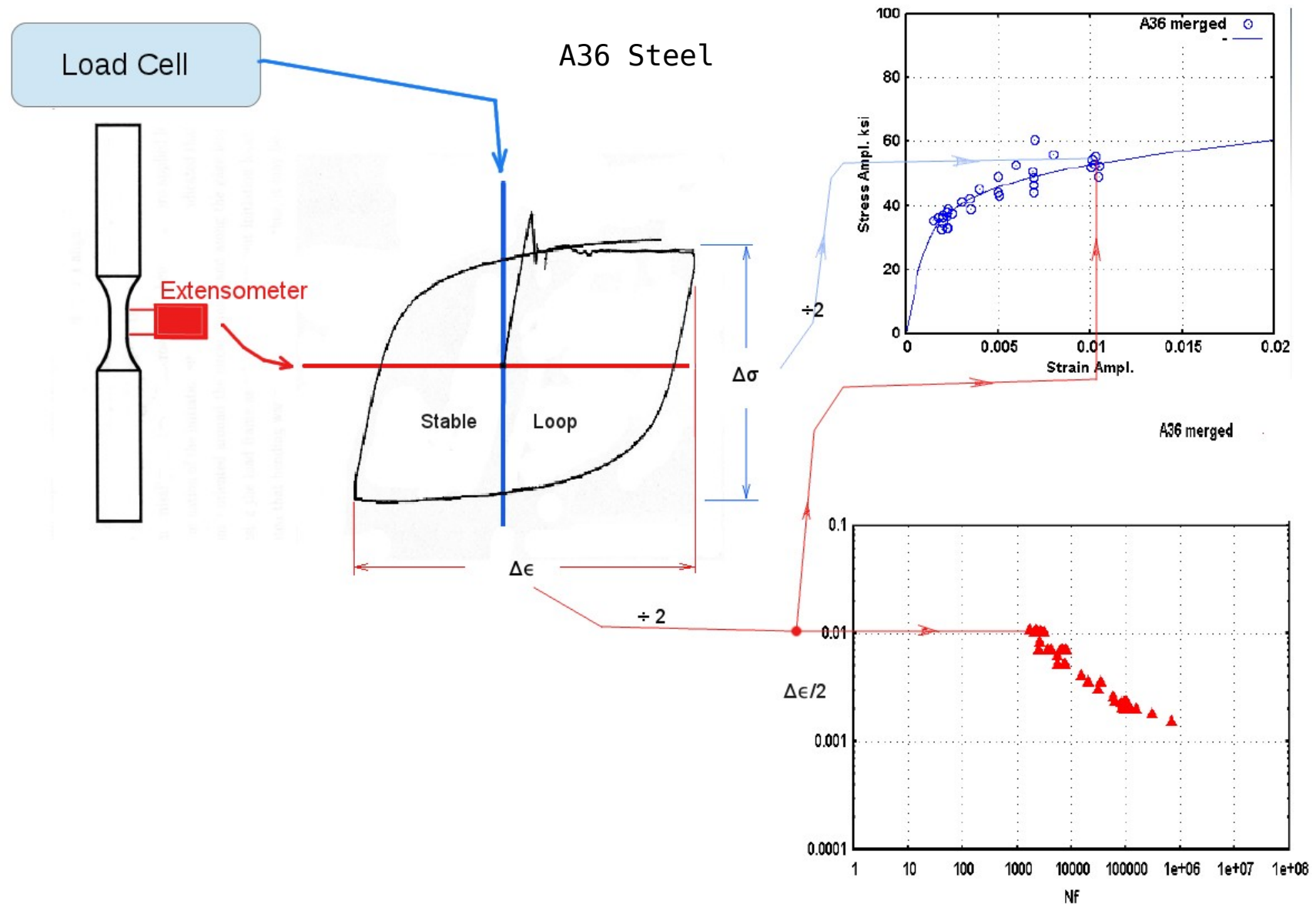
Decreasing in this case.

This material cyclically softens. Plasticity is altering its microstructure



We need to record and graph stress, strain and life for this test.

The stress amplitude  $\Delta\sigma/2$  is taken from the half life hysteresis loop.





In our simulated Boron Steel test we would record the stress, strain, and life in a text file of SAE Standard format:

Here is our  
test

```
#FileType= strain_life
#DataType= raw
#TIMEcol= 0
#NAME= UoWaterloo
#NAME= SAE10B20_Steel
#Stress_units= ksi
#Strain_units= strain
#Su= 121.00
#Sy= 110.00
#E= 30000.
#%RA= 0.0 Not reported
#BHN= 231.
#NO. FAT. PTS.= 12
#Tot Strain 2Nf Stress Mean Plas.Strain Initial
## Amp Amp Sts Amp ElasticMod.
0.024650 425. 104.00 0. 0.021180 30000. #Diametral
0.010000 2031. 92.00 0. 0.006930 30000.
0.007950 3076. 88.00 0. 0.005020 30000.
0.006900 4283. 83.00 0. 0.004130 30000.
0.005830 6201. 80.00 0. 0.003160 30000.
0.004920 10611. 79.00 0. 0.002290 30000.
0.003710 28893. 76.50 0. 0.001160 30000.
0.002900 98546. 73.00 0. 0.000467 30000.
0.002850 100012. 71.50 0. 0.000467 30000.
0.002780 92800. 73.00 0. 0.000347 30000.
0.002440 417400. 70.00 0. 0.000107 30000.
0.002210 9661220. 67.00 0. 0.000000 30000. #Runout
```

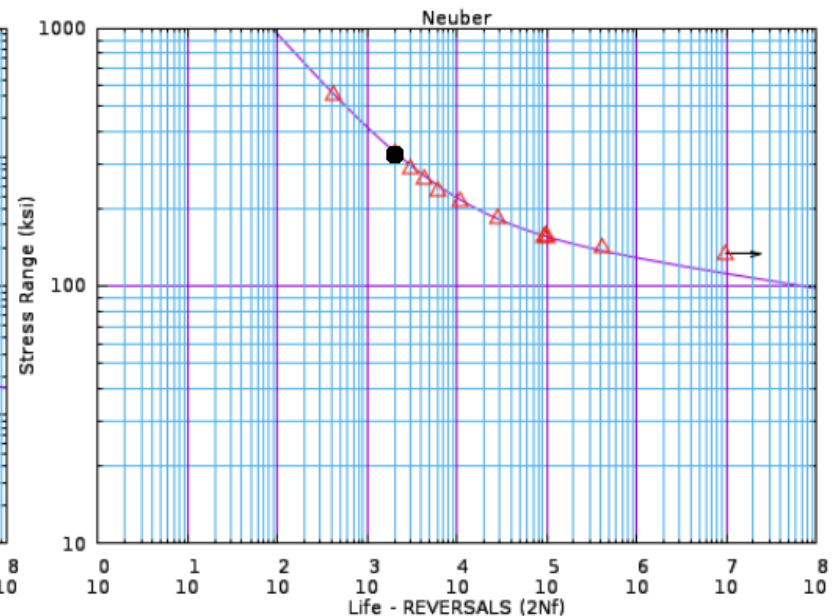
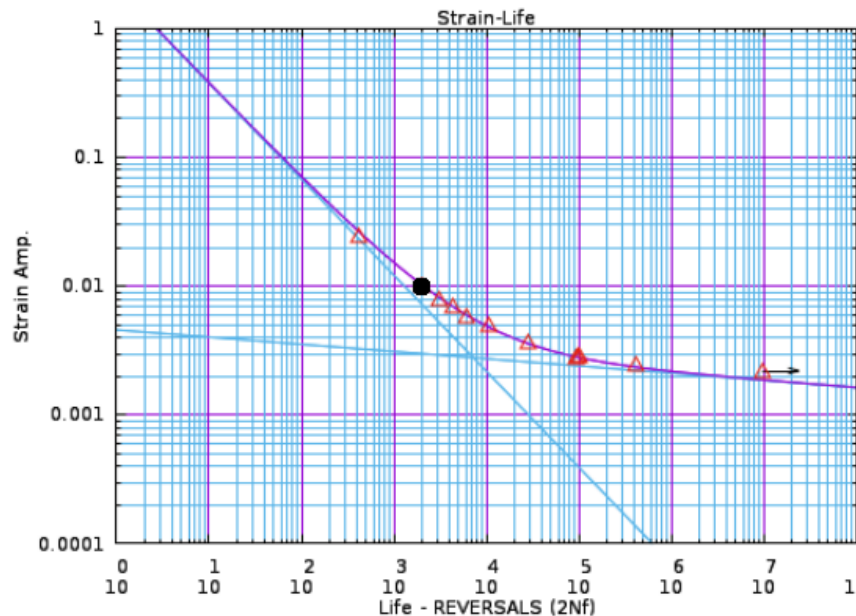
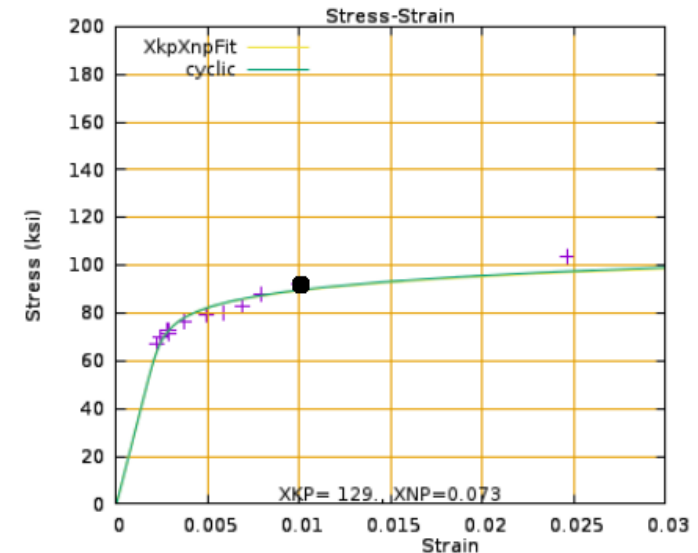
While the tests are underway you will probably only need to plot the Strain Ampl. vs 2Nf. When all are done make these three plots.  
( more on this later )

Our point in Black

UoWaterloo SAE10B20<sub>s</sub> BHN= 231

# SAE10B22 quenched + temp to Rc=35. The 1/2in  
# plate was retempered at 1020F for 3hrs to avg. core hardness  
# of Rc=21. Material supplied by Caterpillar Tractor Co.  
# Cylindrical spec., 0.3in GL, parallel to roll dir.,  
# ground + polished after machining.  
# SAE10B20 chemistry 0.20C 1.32Mn .009P .010S .27Si .01Ni  
# .02Cr .01Cu .05Al .050Ti 0.00096Boron  
# Sample with 425 life is a diametral test.  
# Ref.: F.A.Conle, 'A Computer Simulation Assisted Statistical  
# Approach to the Problem of Random Fatigue,' MSc Thesis  
# Univ. of Waterloo, March 1974  
# Amp      Amp      Stress      Amp      Elastic Mod.

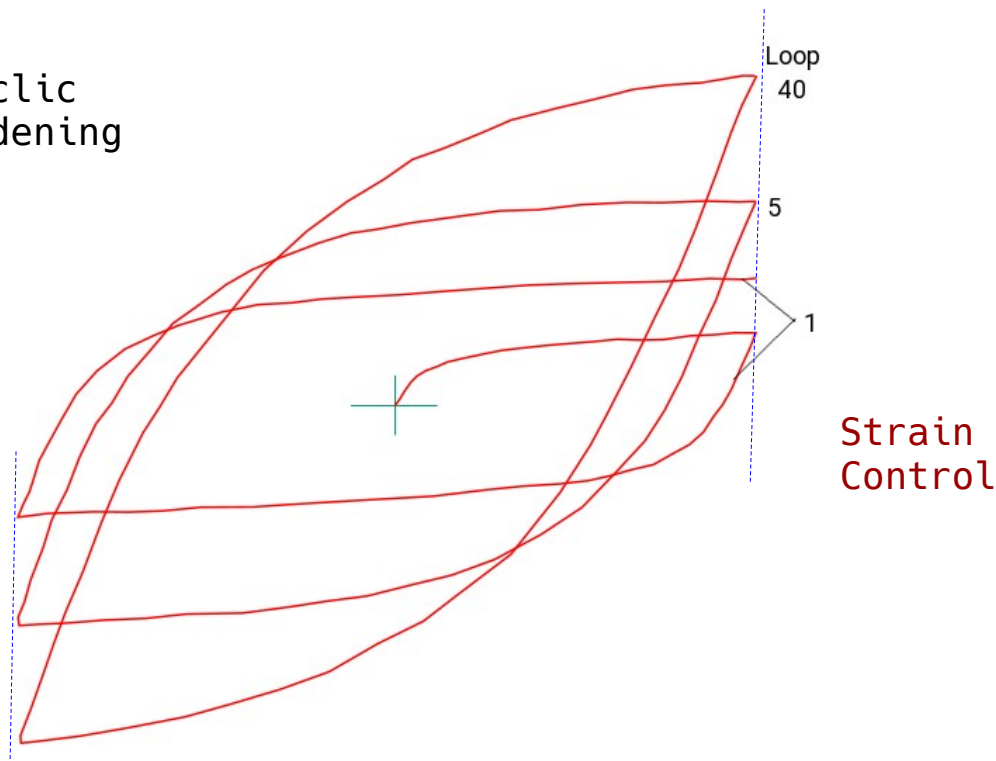
|                                   |                                   |               |  |
|-----------------------------------|-----------------------------------|---------------|--|
| Monotonic Props.                  |                                   | Cyclic Props. |  |
| ELAS. MOD. = 30000. KSI, 207. GPa | K' = 130.1 KSI, 897.MPA           |               |  |
| YIELD, 0.2% = 110. KSI, 758. MPA  | N' = 0.0751                       |               |  |
| ULT. STRG. = 121. KSI, 834. MPA   | F. STRG COEF = 137.6 KSI, 948.MPA |               |  |
| K = 0.0 KSI, 0. MPA               | F. STRG EXP, b = -0.0559          |               |  |
| N = 0.0000                        | FAT DUCT COEF = 2.0907            |               |  |
| RED. IN AREA = 0.0                | F. DUCT EXP, c = -0.7450          |               |  |
| T. FRAC. STG. = 0.0 KSI, 0. MPA   | Exp Cyc Yld = 82. Ksi, 563.MPA    |               |  |
| T. FRAC. STR. = 0.000             | Fit Cyc Yld = 82. Ksi, 563.MPA    |               |  |
| No. data points = 12              |                                   |               |  |



# Cyclic Hardening and Softening

In a previous slide it was mentioned that we use the “**Stable**” **stress-strain hysteresis loop** to plot a test’s stress or strain amplitude. Typically the loop observed at  $\frac{1}{2}$  Life is assumed stable. This measure is needed because materials can harden or soften when fatigue cycles are imposed.

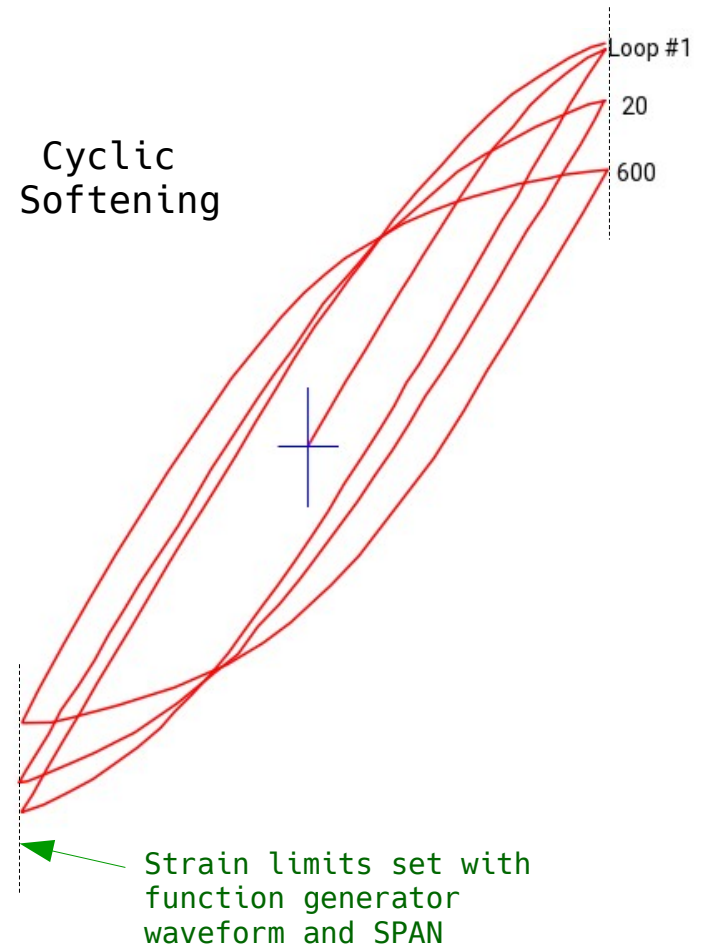
Cyclic Hardening



Video 5Mb

<https://fde.uwaterloo.ca/FatigueClass/Videos/ohfcAnnealed.gif>

Cyclic Softening



Video 5Mb

<https://fde.uwaterloo.ca/FatigueClass/Videos/ohfcCWorked.gif>

## Why use Strain Control?

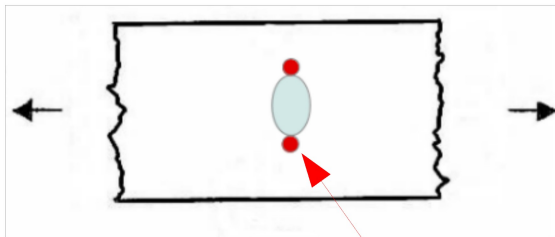
Primarily because of plasticity and cyclic hardening or softening

In this test the steel is initially elastic (Loop 1) and max load is below Yield.

After some cycles the energy input is sufficient to release the pinned dislocations, and the loop "Pops open"

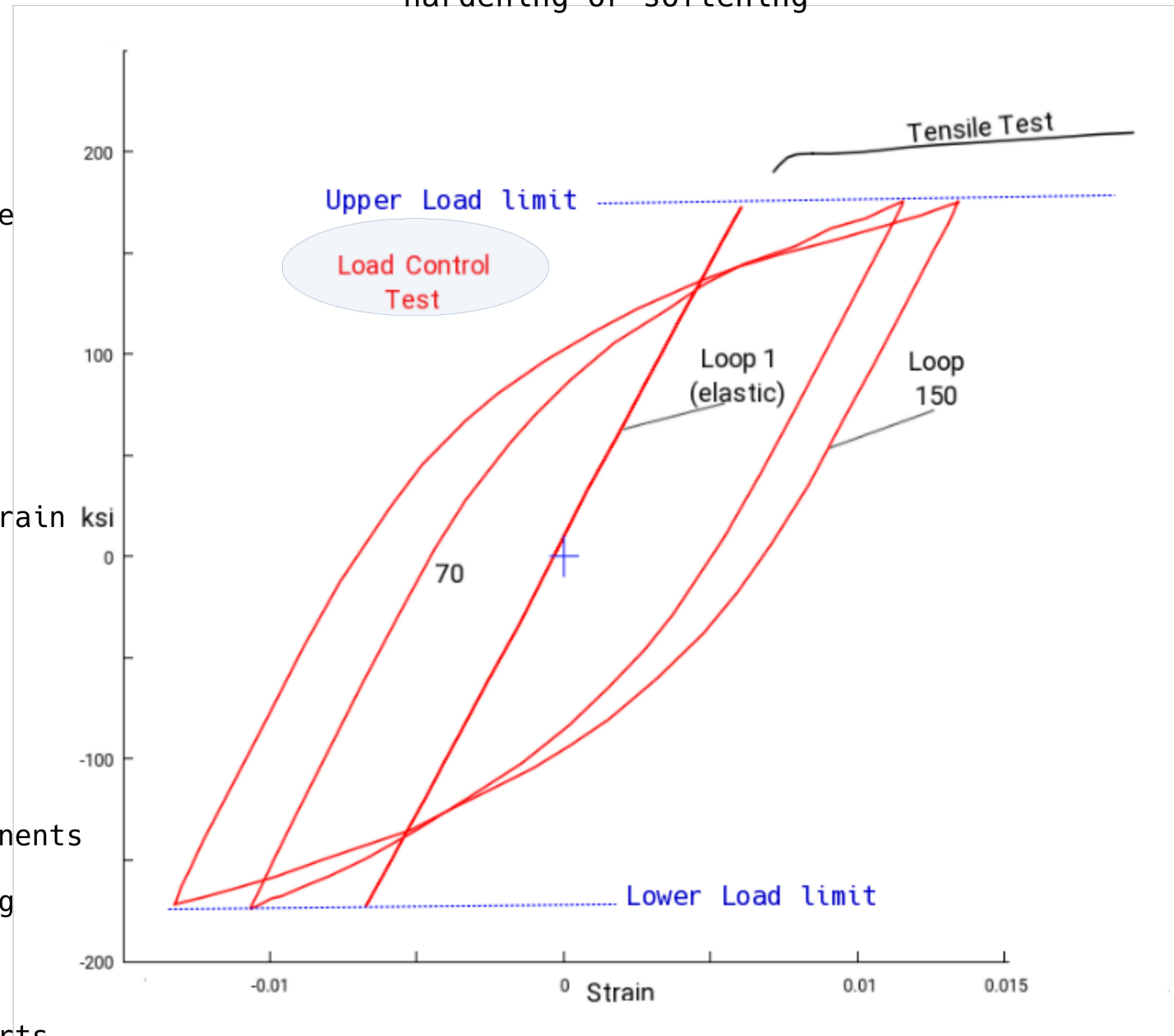
With additional cycles and cyclic softening the loops get very large.

If the upper load limit was above the yield the stress-strain could fracture the sample.



This does not happen in components where the fatigue **hot-spot** is constrained by the surrounding elastic structure.

Thus strain control is closer to conditions seen in real parts.



Here is a video of some of the stress-strain loops of the previous slide:

Video: <https://fde.uwaterloo.ca/FatigueClass/Videos/allsa1045Loops.gif> 8Mb

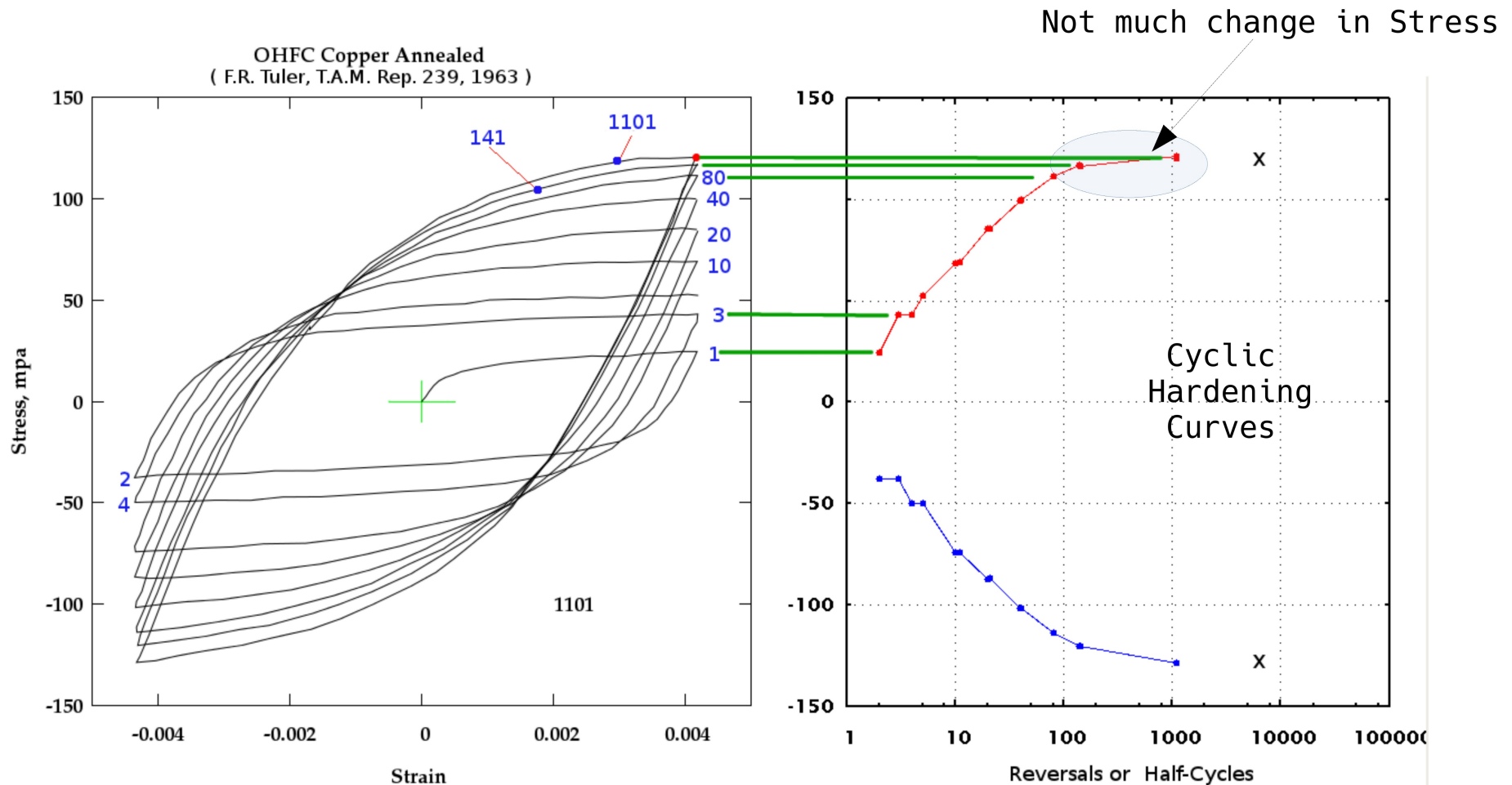
**Note** that in the first 20 cycles that there is little or no plasticity.

Suddenly around cycle 50 the loops “open up” and start to show some plasticity. One of the explanations is that the seemingly elastic cycles are actually imparting some energy into the steel Fe-C lattice, and given enough the dislocations that have been previously pinned by the carbon atoms are set free to move and multiply.

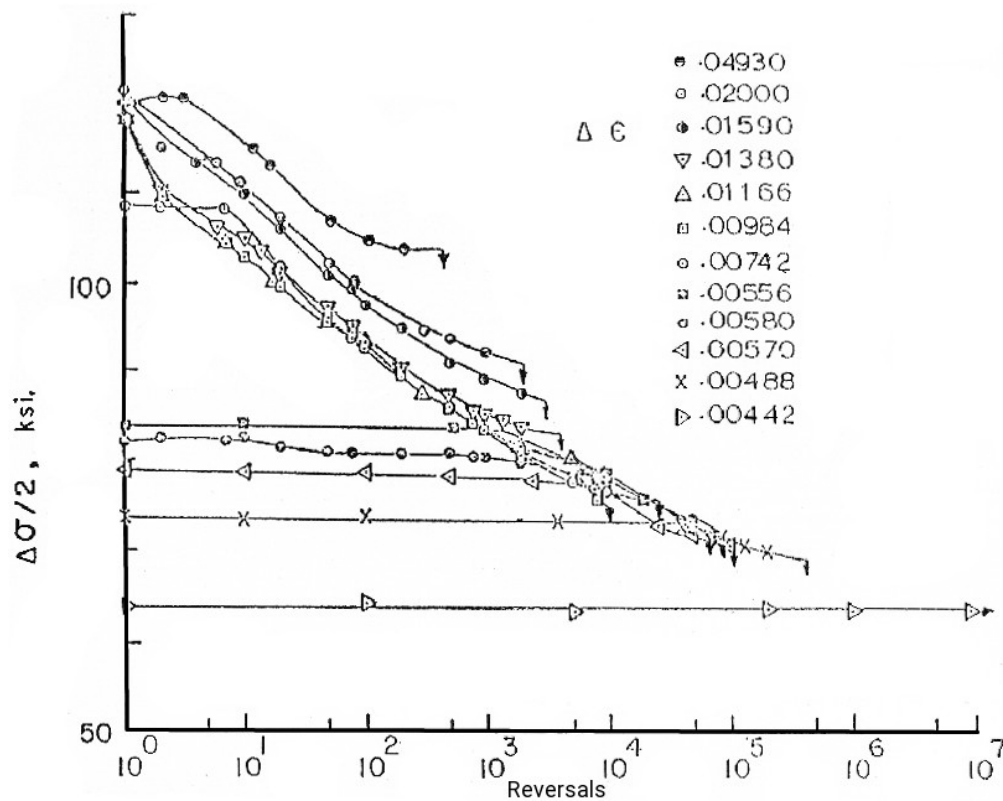
This behavior is seen in many steels that cyclically soften. It is one of the reasons that simple tensile test information is not enough for fatigue design.

For each strain controlled test one can collect the stress response and create a “Cyclic Hardening” (or softening ) plot.

Note that the X axis is logarithmic, and that for this test there is not a big difference between stress amplitude at reversal 140 and reversal 1101. This steady state comprises most of the test life. One can conclude from this that  $\frac{1}{2}$  Life stress ampl. is representative of a fatigue test at this strain amplitude.







For any fatigue analysis that requires the stress-strain relationship one should use the cyclic stress-strain curve.

By plotting the half-life stress values for this Boron Steel vs. the test strain amplitudes the cyclic stress-strain curve can be contrasted with the tensile test result.

This material shows a drastic difference

